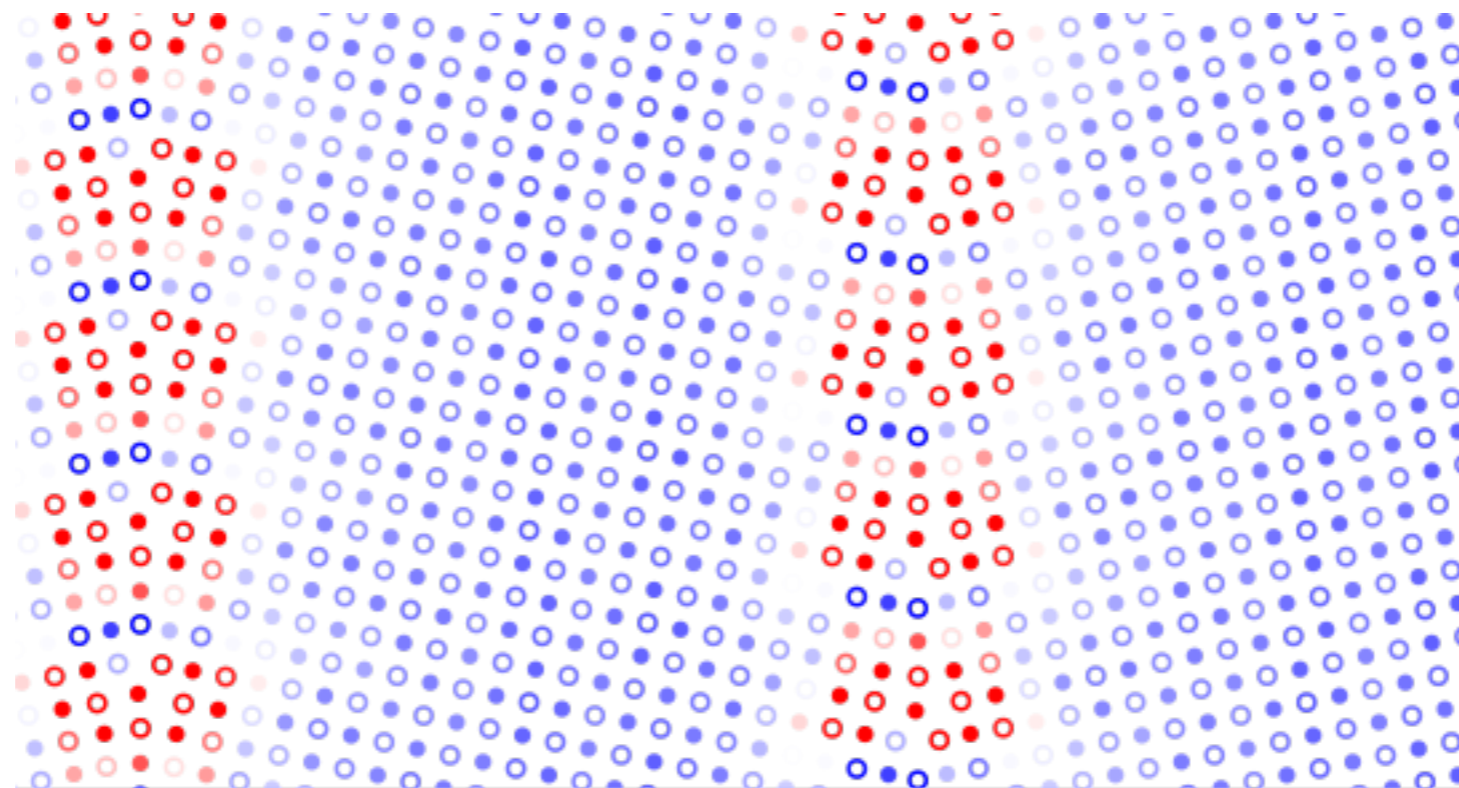


第8回 IFERC-CSC研究会

2018.2.27-3.1

ビジョンセンター日本橋 本館5階501号室

# Cuの粒界エネルギーの 精密計算



POSCAR\_0\_121215\_468\_inner\_relax\_-2\_0

関西学院大学・理工学部・西谷滋人

# contents

- Theoretical, experimental and simulated
  - Read and Shockley's theoretical prediction
  - Otsuki's experimental results
  - Others(experimental and calculated)
- First principles(VASP) calculations
  - Al, Cu
- EAM analysis
- Conclusions

# Read and Shockley Theoretical Predictions

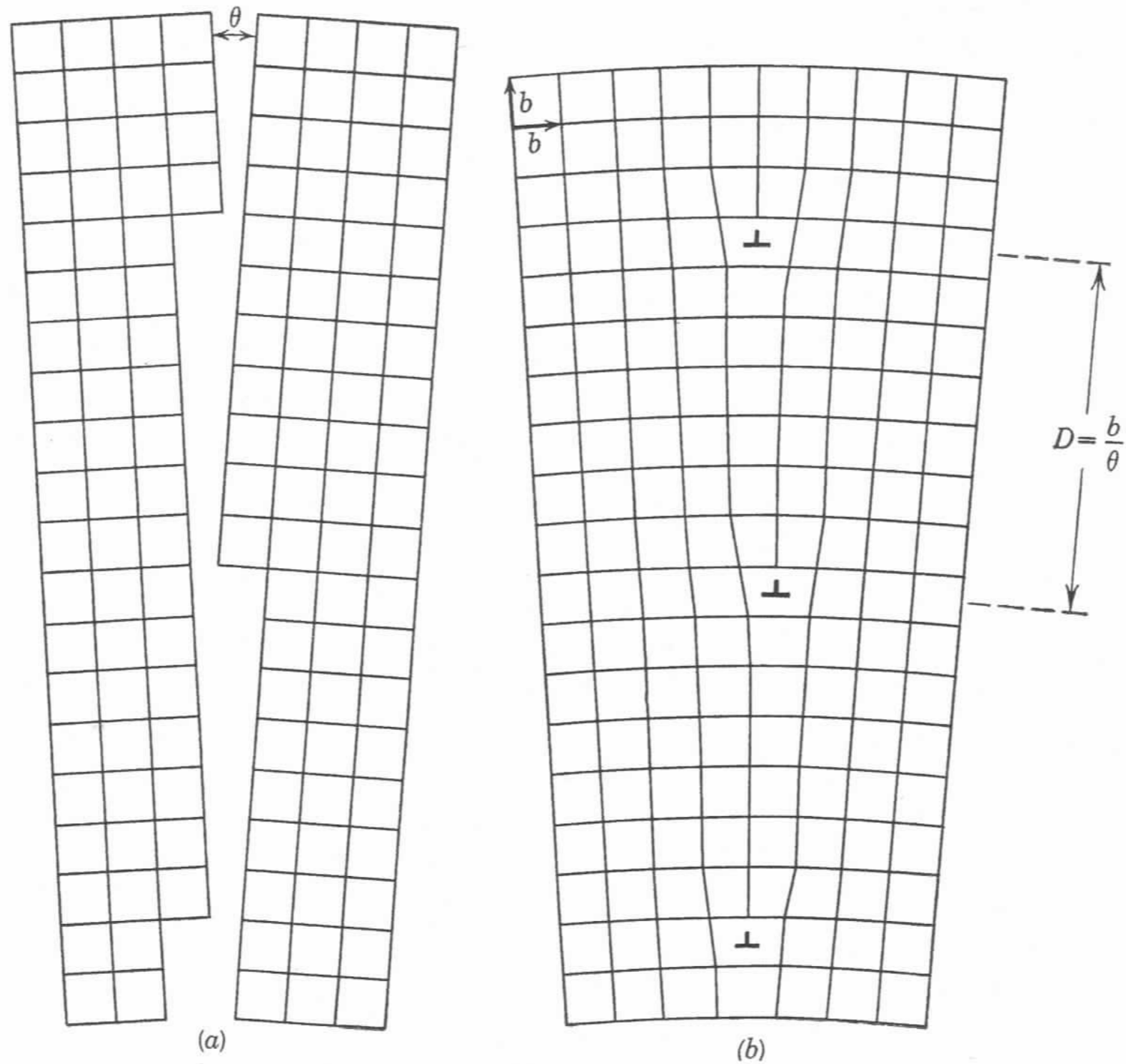
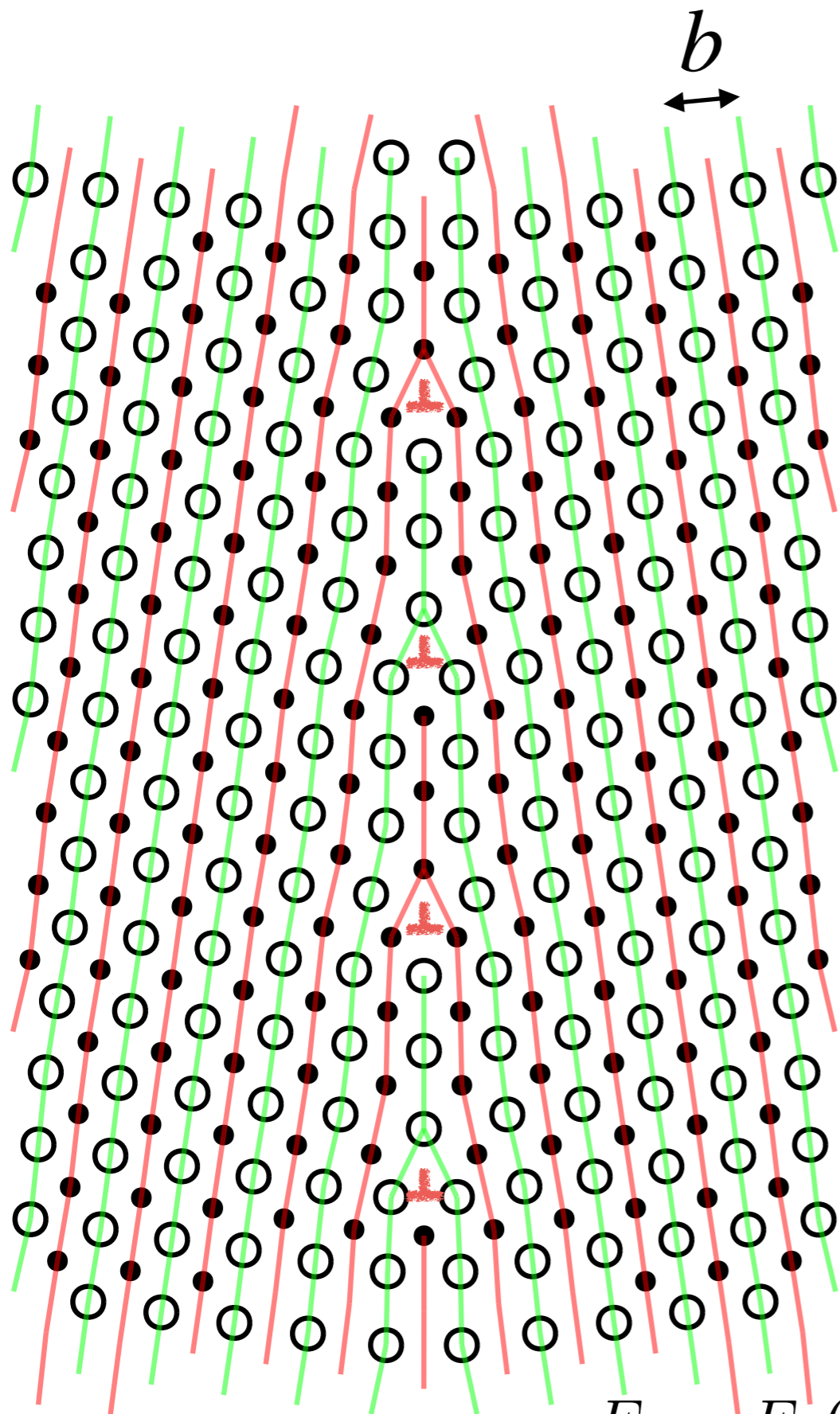
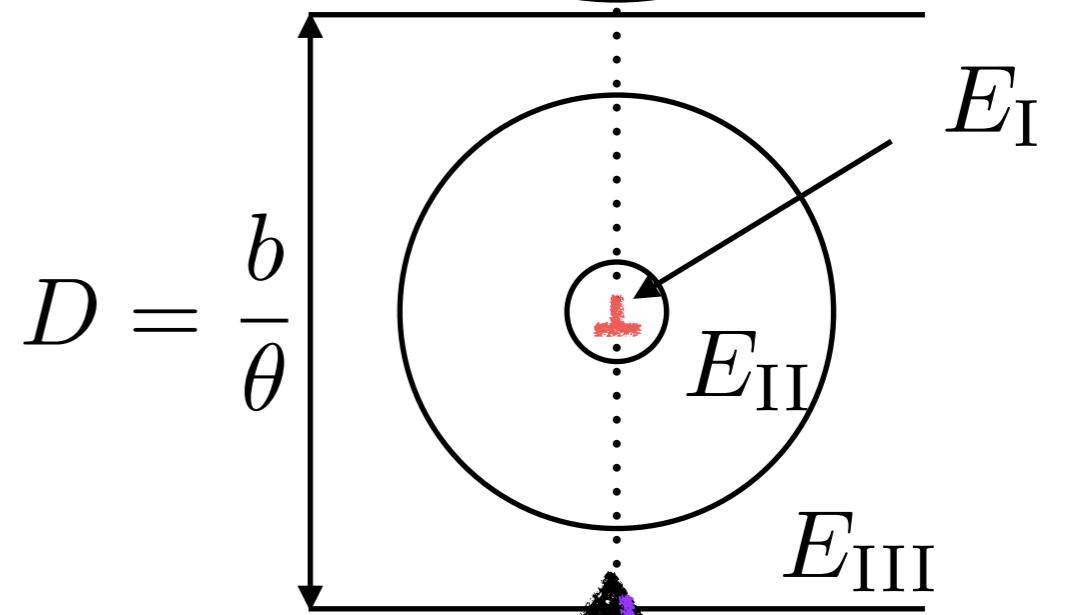
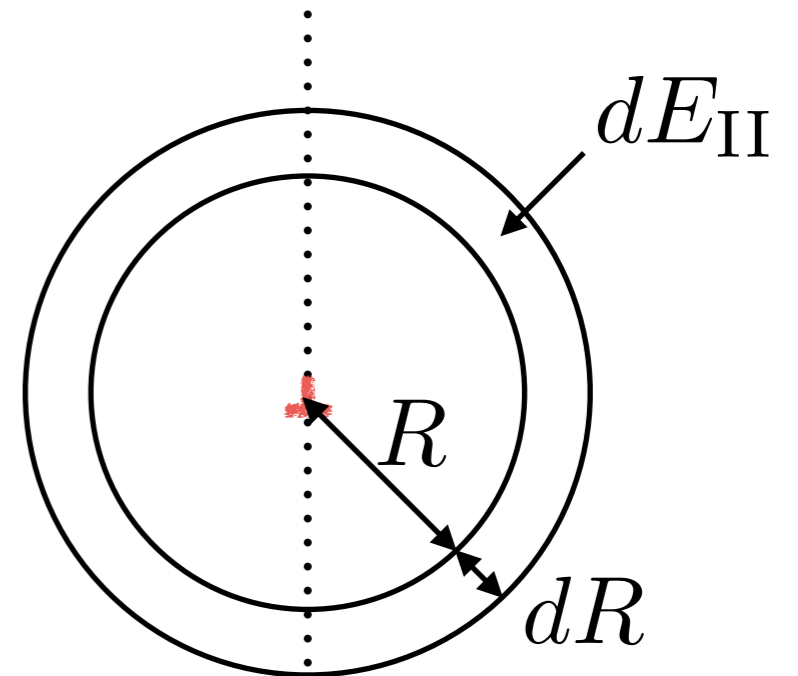


FIG. 1. Simple grain boundary showing (a) two grains with common crystal axis and (b) method of joining and dislocation model.

"Dislocation Models of Grain Boundaries", W. T. Read Jr., and W. Shockley,  
 "Imperfection in nearly perfect crystals", ed. by W. Shockley, chap.13,  
 (Wiley, New York, 1952) p.352-376.

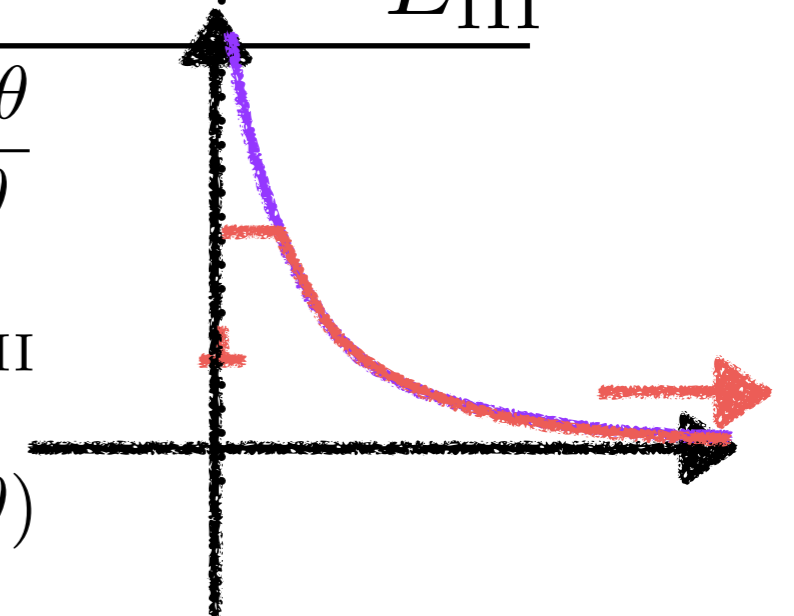


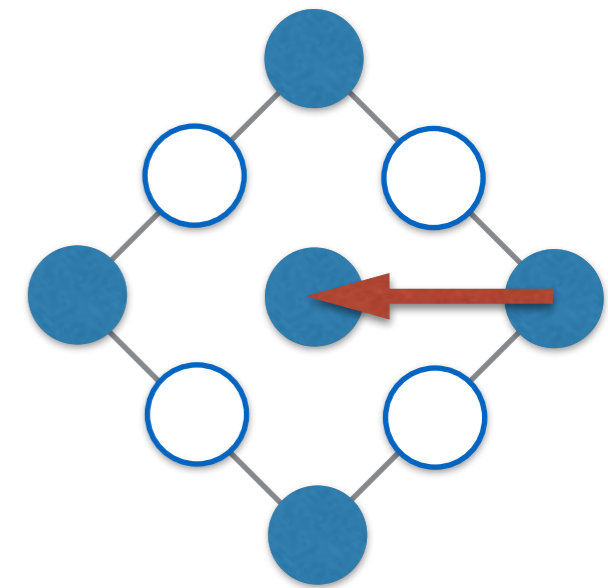
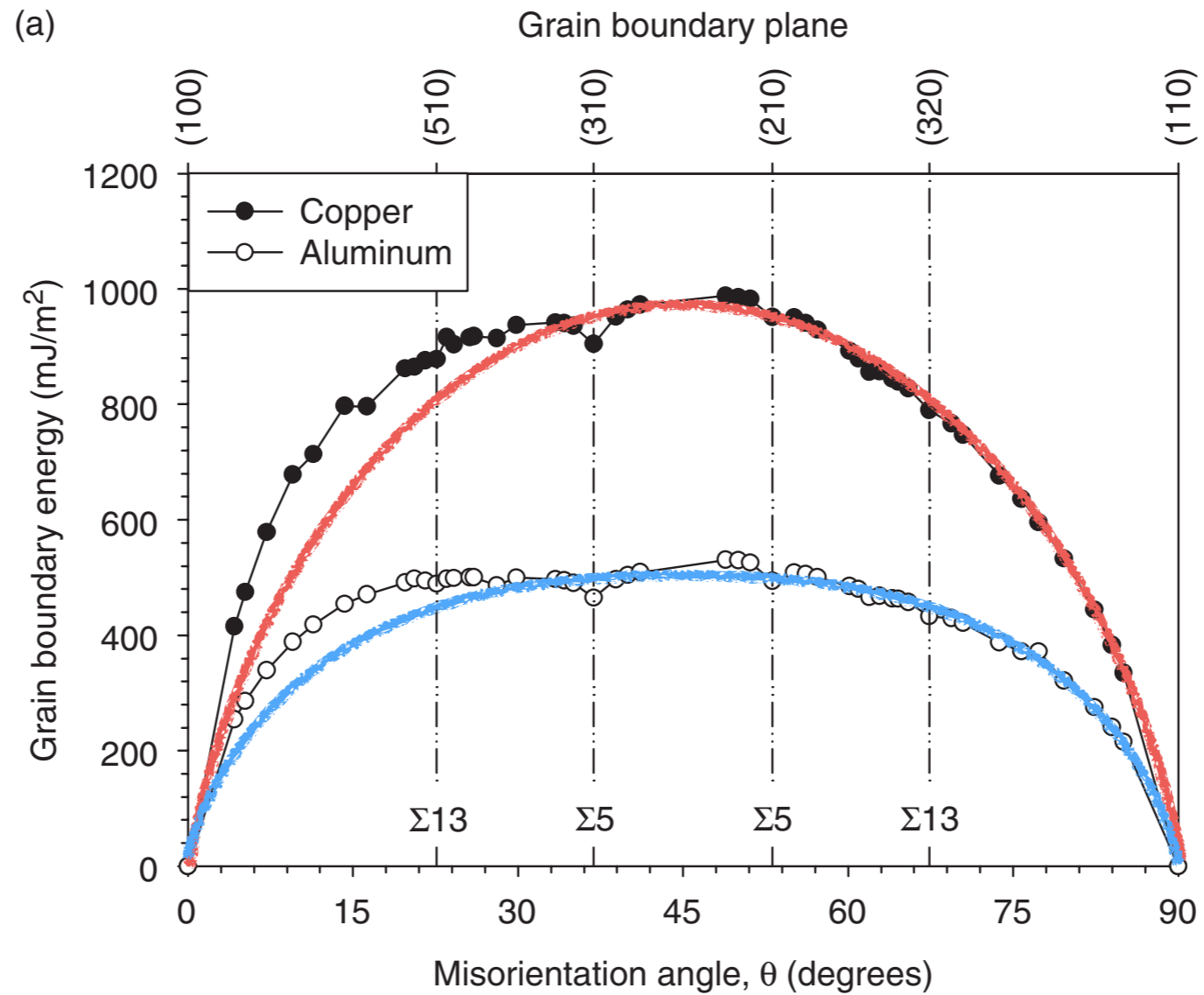
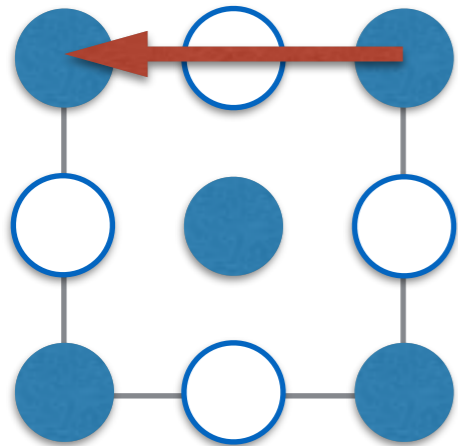
$$E_b = E_d \theta / b \underset{5}{=} E_0 \theta (A - \log \theta)$$



$$dE_{II} = -\frac{b^2 \tau_0}{2} \frac{d\theta}{\theta}$$

$$E_d = \int_{r_{\text{core}}}^{r_\theta} dE_{II}$$





"Asymmetric tilt grain boundary structure and energy in copper and aluminium",  
M. A. Tschopp and D. L. McDowell, *Phil. Mag.*,  
Vol. 87 (2007), 3871–3892.  
They used EAM potentials.

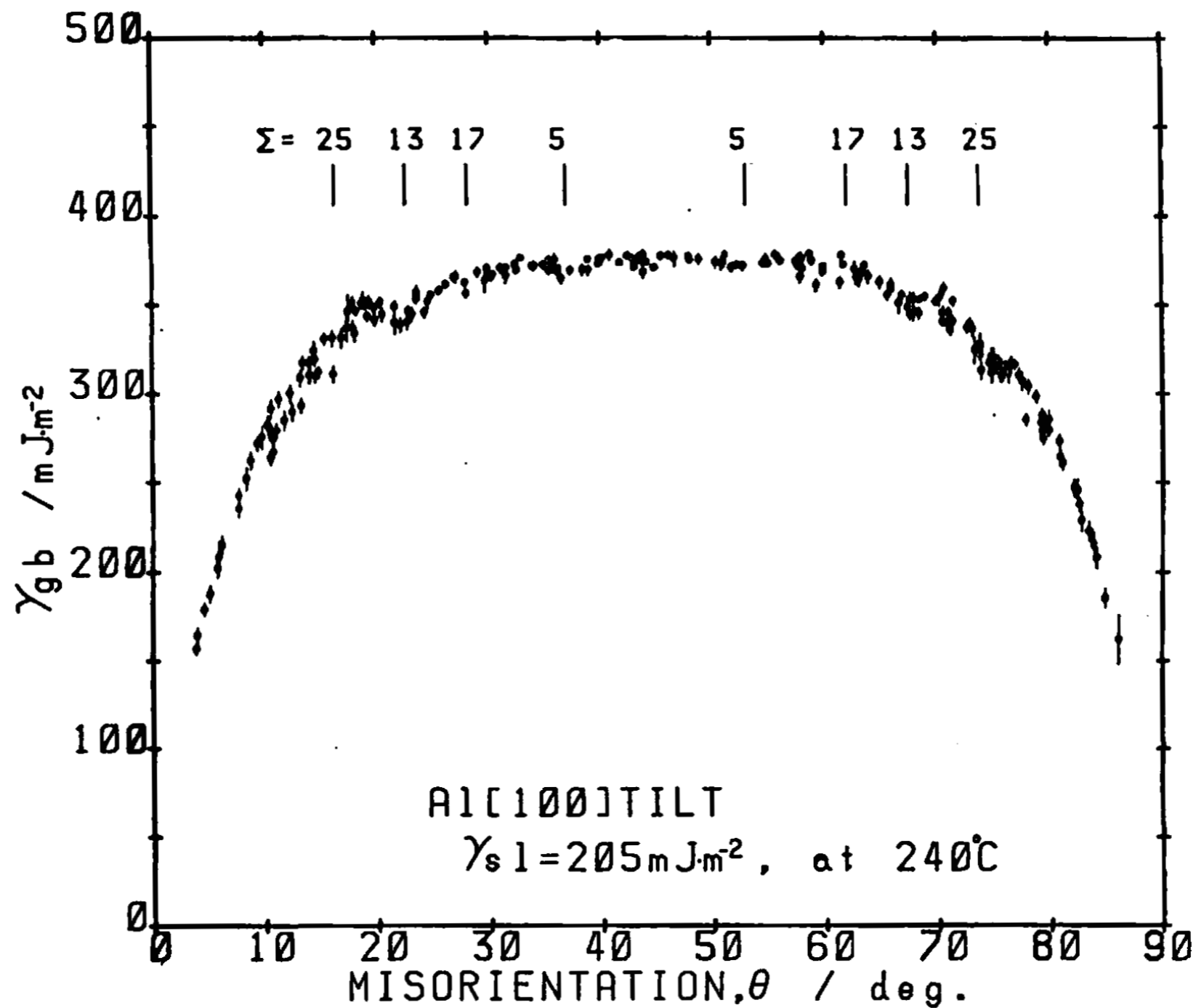
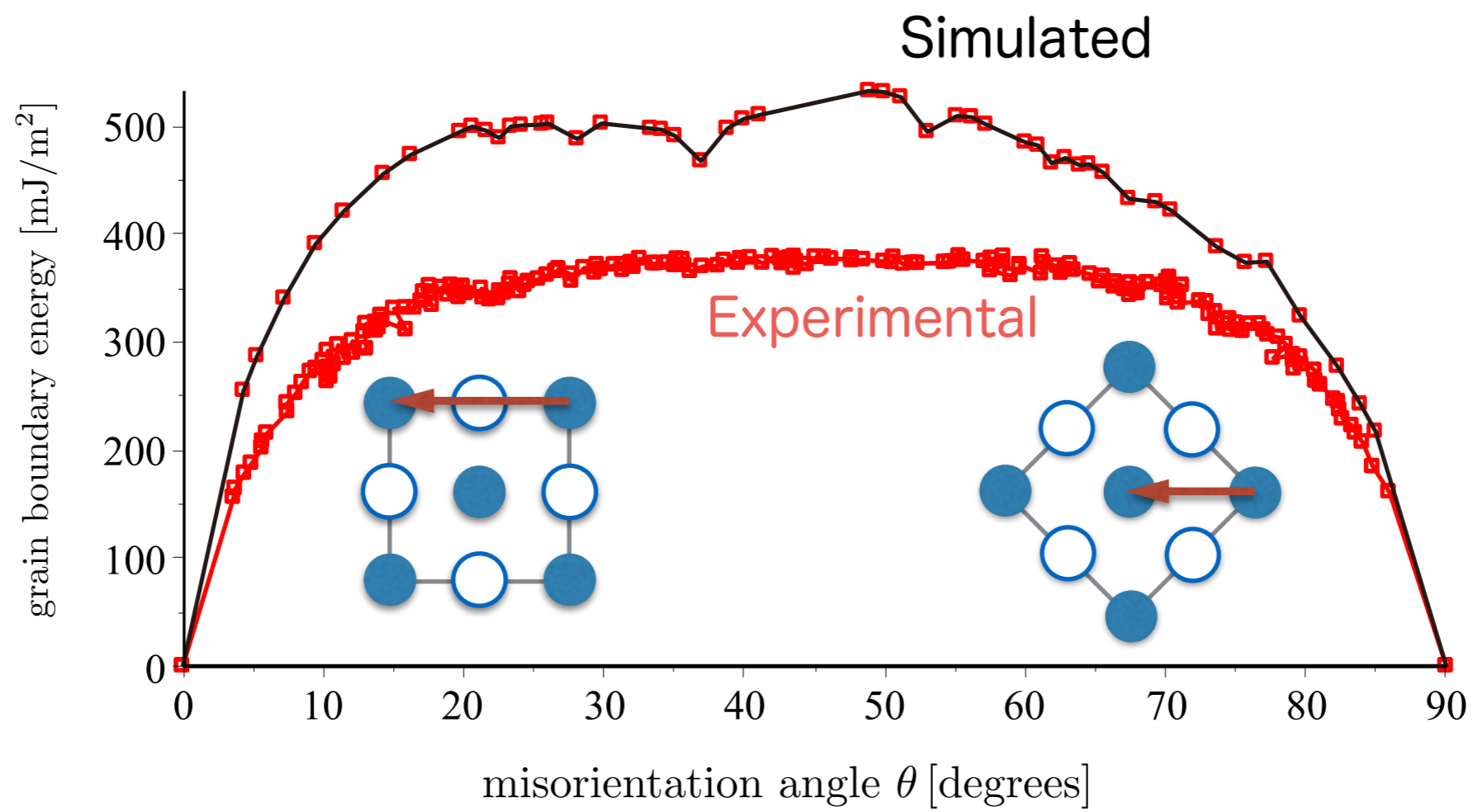


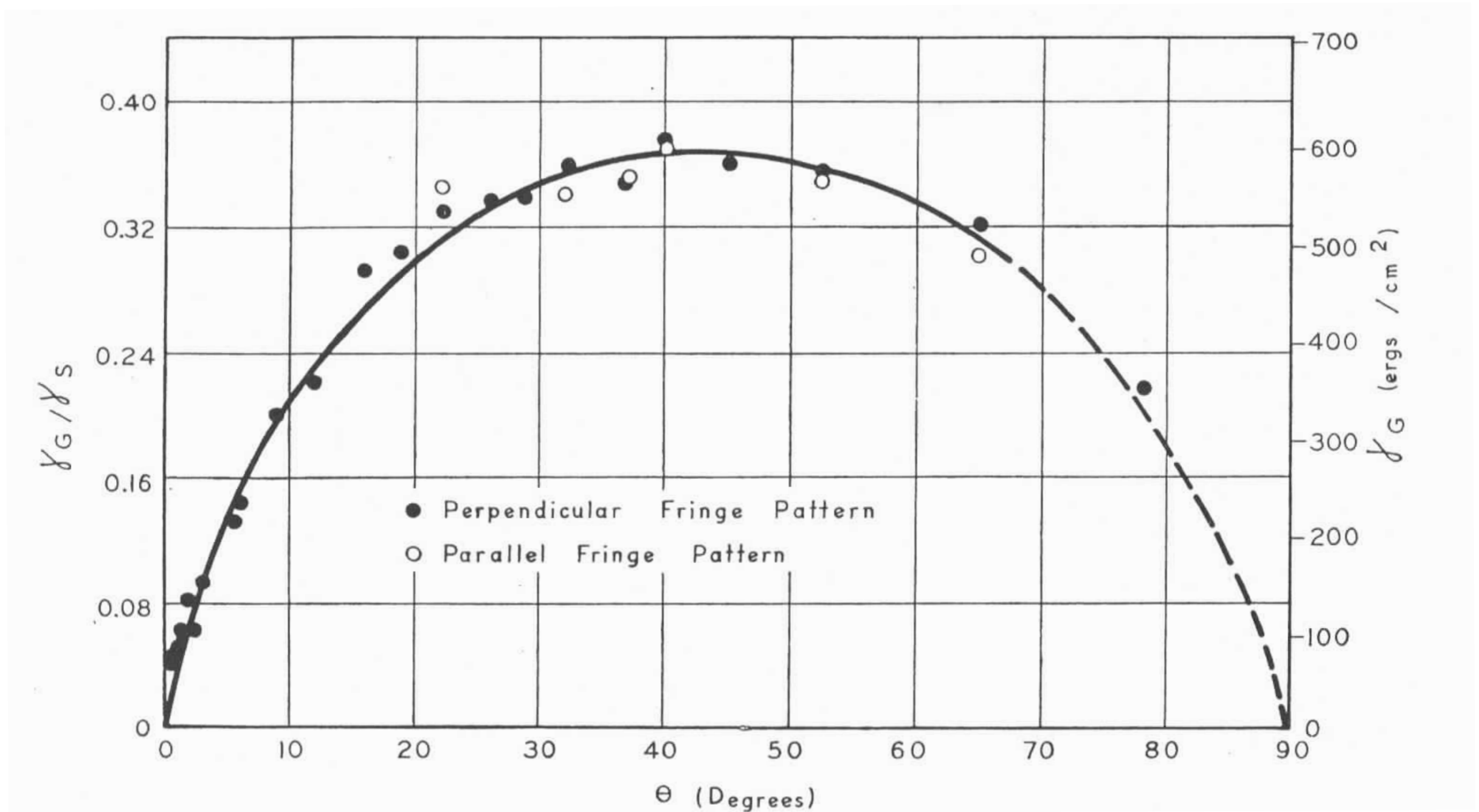
Fig.5-9 Grain boundary energy,  $\gamma_{gb}$ , as a function of  $\theta$  for Al[100] tilt boundary, where  $\gamma_{sl} = 205 \text{ mJ}\cdot\text{m}^{-2}$ .

“アルミニウムの粒界エネルギーに関する研究”,大槻, 徴  
 (京都大学, 1990-07-23), 博士論文, p.115.

A. Otuki, J. Material Science, 40(2005), 3219.







“Absolute interfacial energies of [001] tilt and twist grain boundaries in copper.”

N.A.Gjostein and F.N.Rhines, Acta Metallurgica, Vol. 7, May 1959, 319.

Fig.4. Dependencies of grain boundary energy on misorientation for [001] tilt boundaries at 1065C. Solid line represents the curve calculated from equation (1), using the large angle parameters.

G. C. Hasson and C. Goux, Scripta Met., 5 (1971), 889.

Al

Measured

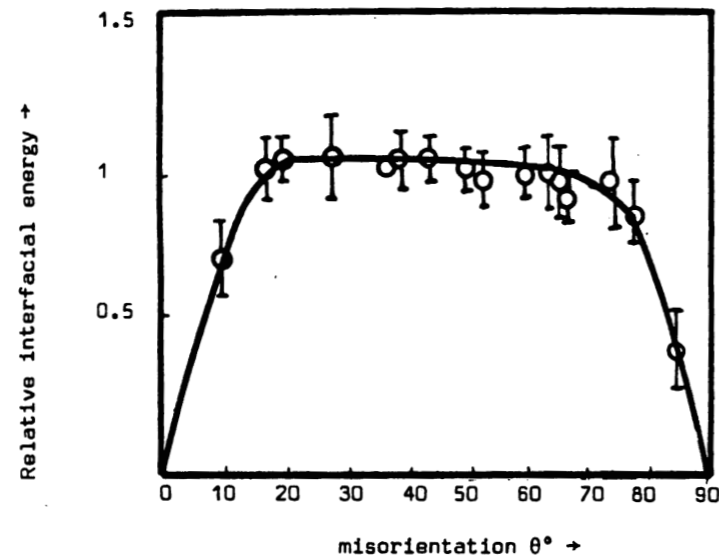


FIG. 1

Measured relative energies of [100] tilt boundaries in aluminium as a function of the misorientation  $\theta$  (between [001] directions). The 37° [100] tilt boundary is used as reference for the energies.

Computed

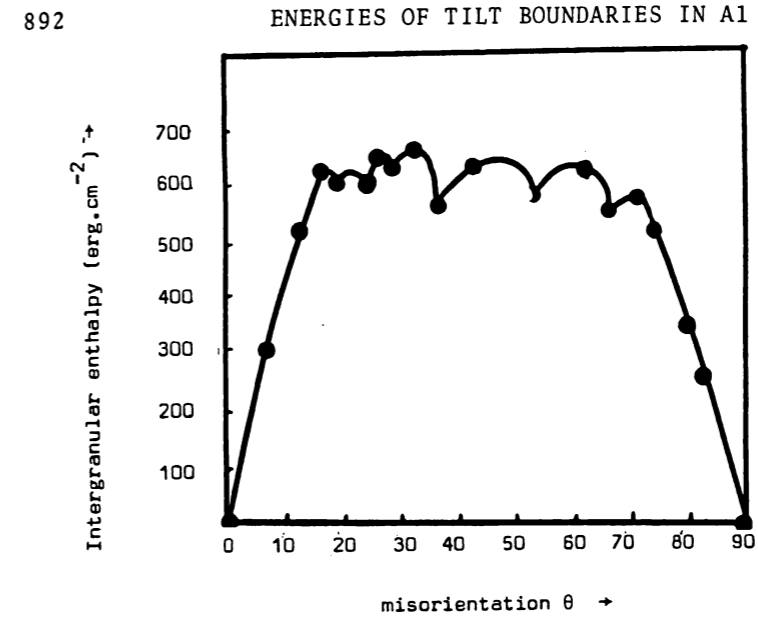
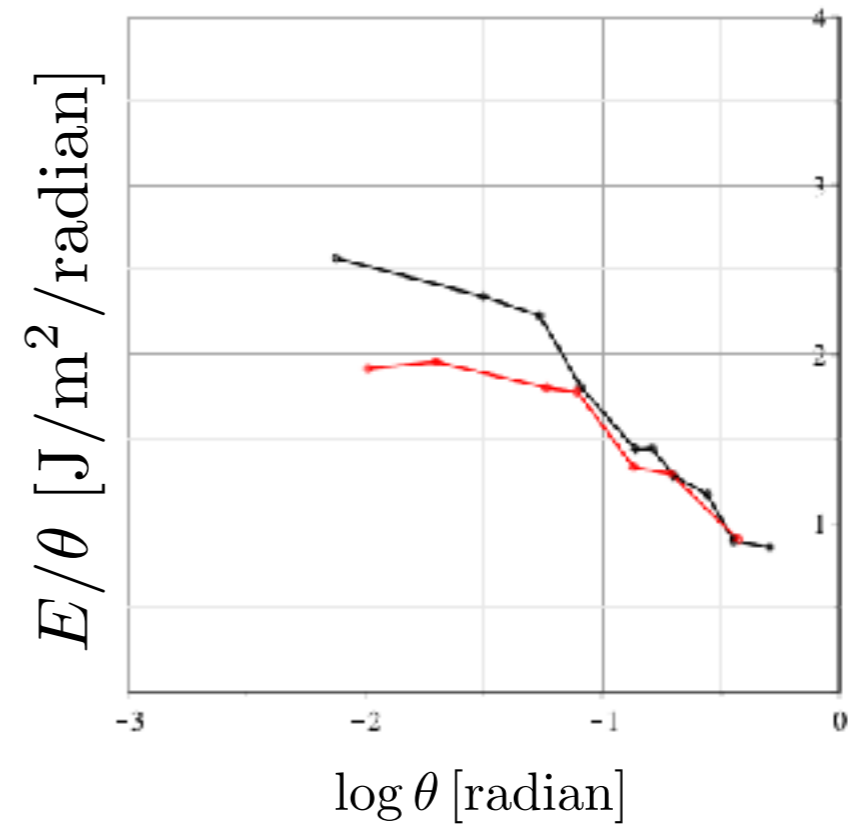
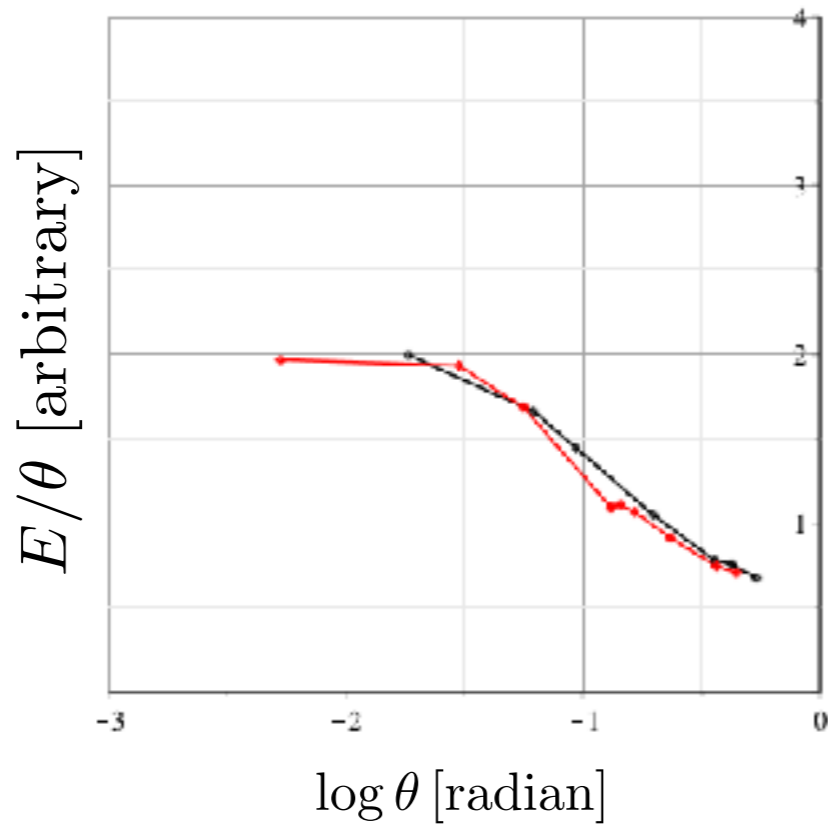


FIG. 3

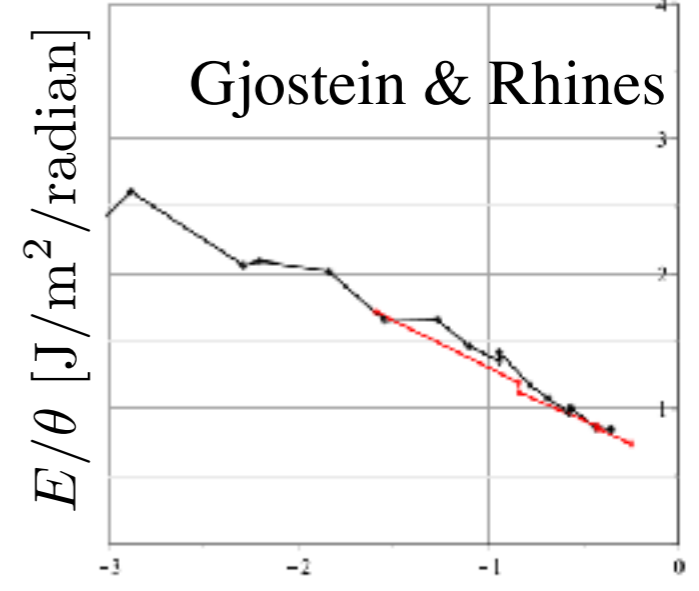
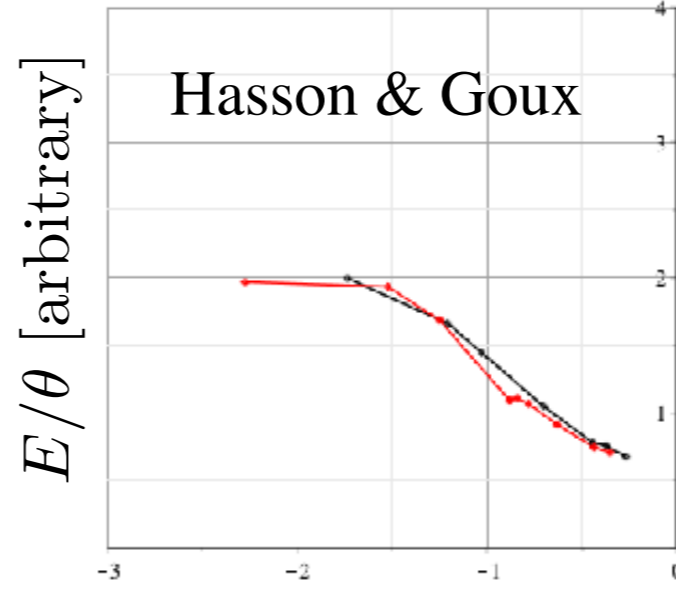
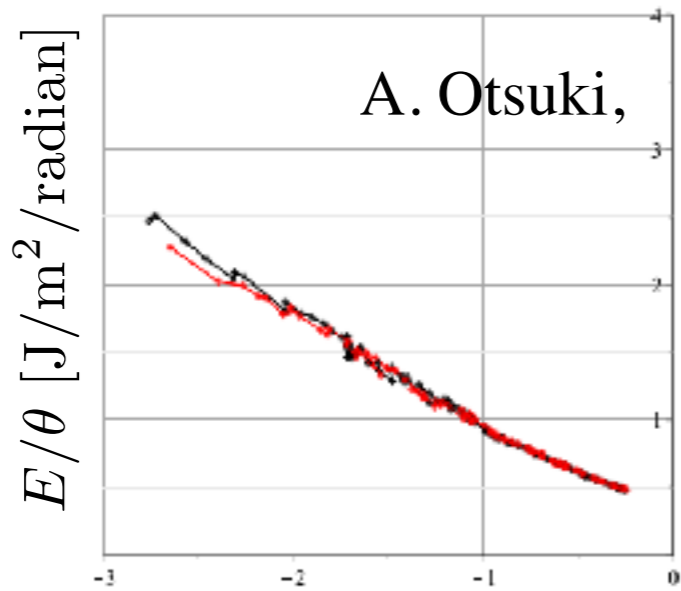
Computed intergranular enthalpy of [100] tilt boundaries in aluminium as a function of misorientation  $\theta$  (between [001] directions)



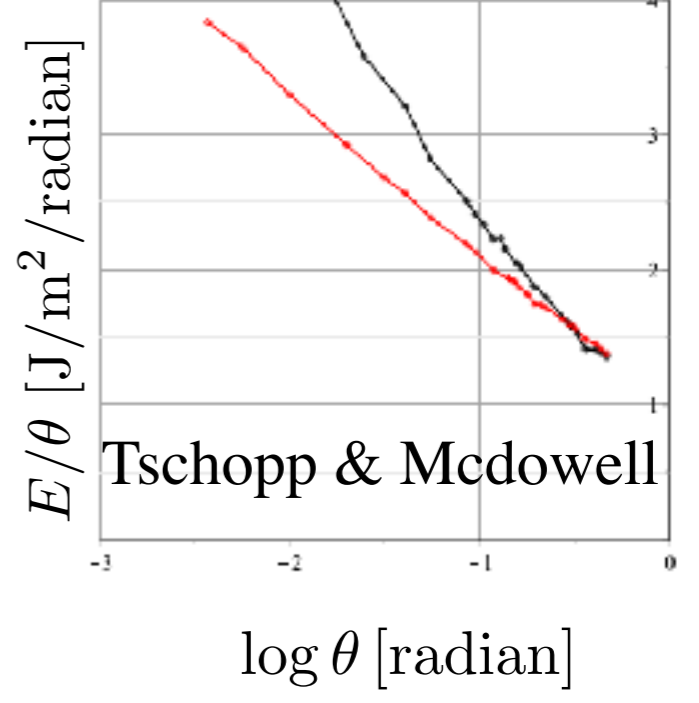
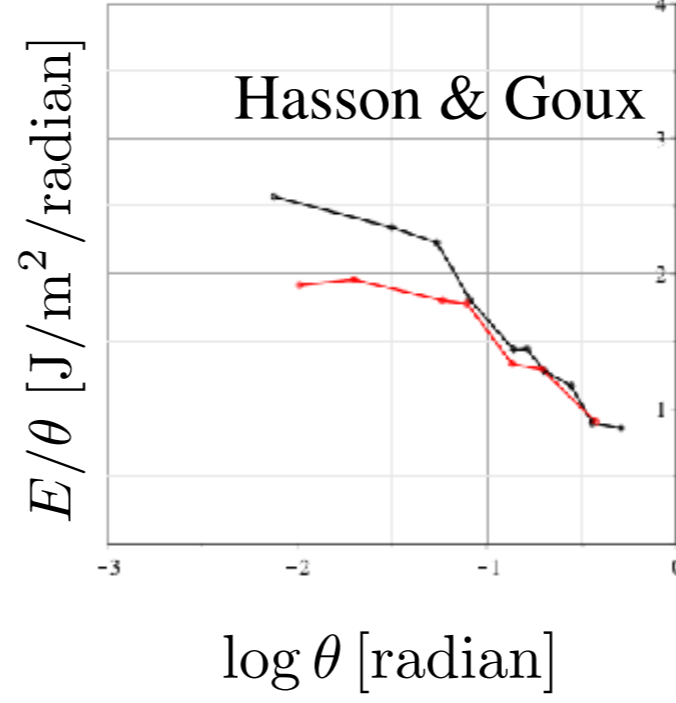
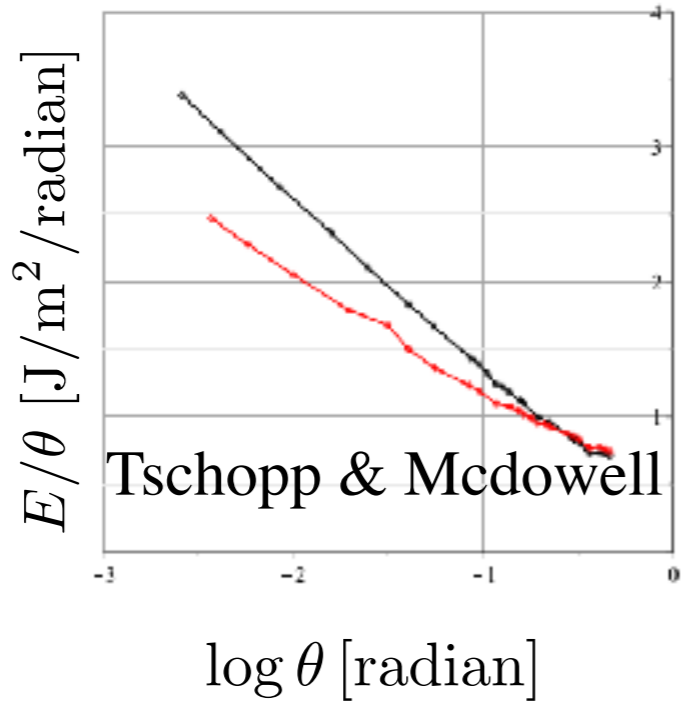
$$E = E_0 \theta (A - \log \theta)$$

$$\frac{E}{\theta} = B - C \log \theta$$

Experimental



Calculated



# VASP calculations for tilt boundaries

Al

# VASP calc. conditions

Pseudo Potential: PAW

Relaxations: outer relax by hand

fix calc after relaxations

INCAR

Energy Cut off: 273.15eV

IBRION = 2 #Relax ions with  
conjugate-gradient

ISIF = 2 #Relax ions, calc stress

EDIFF = 1.0e-05 #criteria for electronic  
SC-loop

EDIFFG = -0.02 #criteria for ionic  
relaxation loop

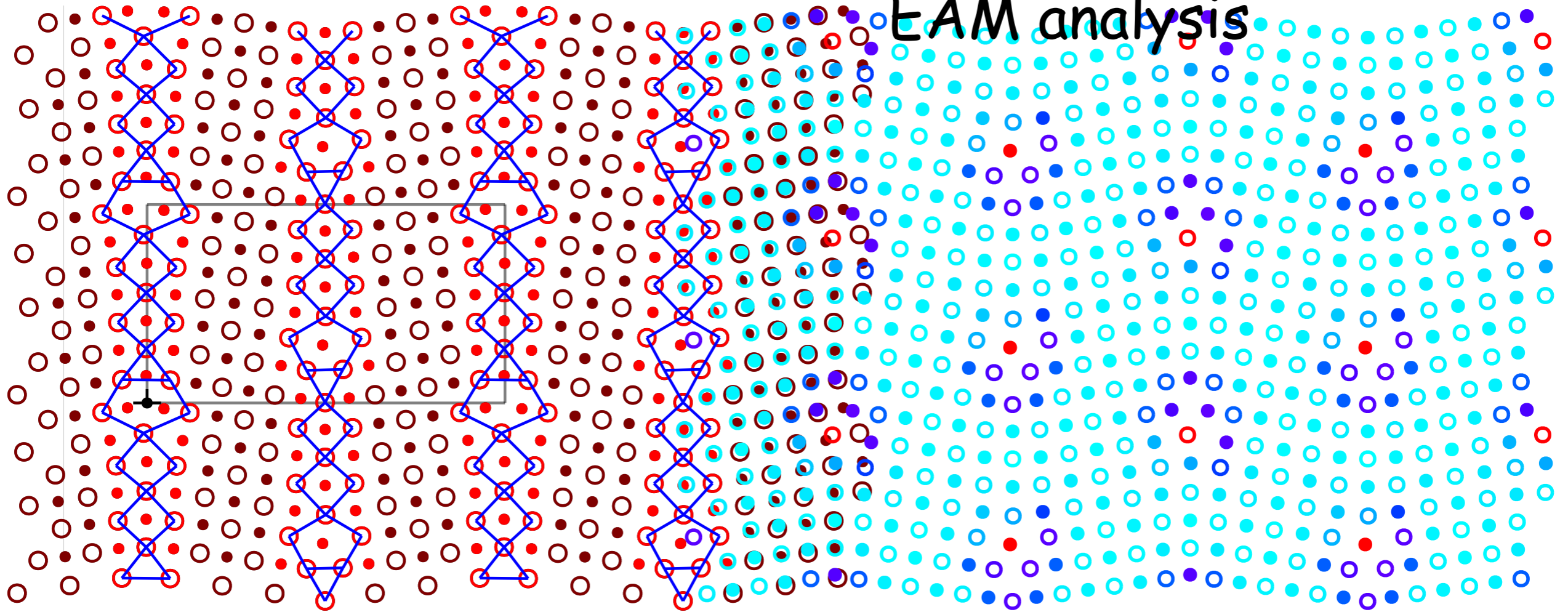
KPOINT

100

Use automatic

length=50 ✓ due to no d-electron for Al

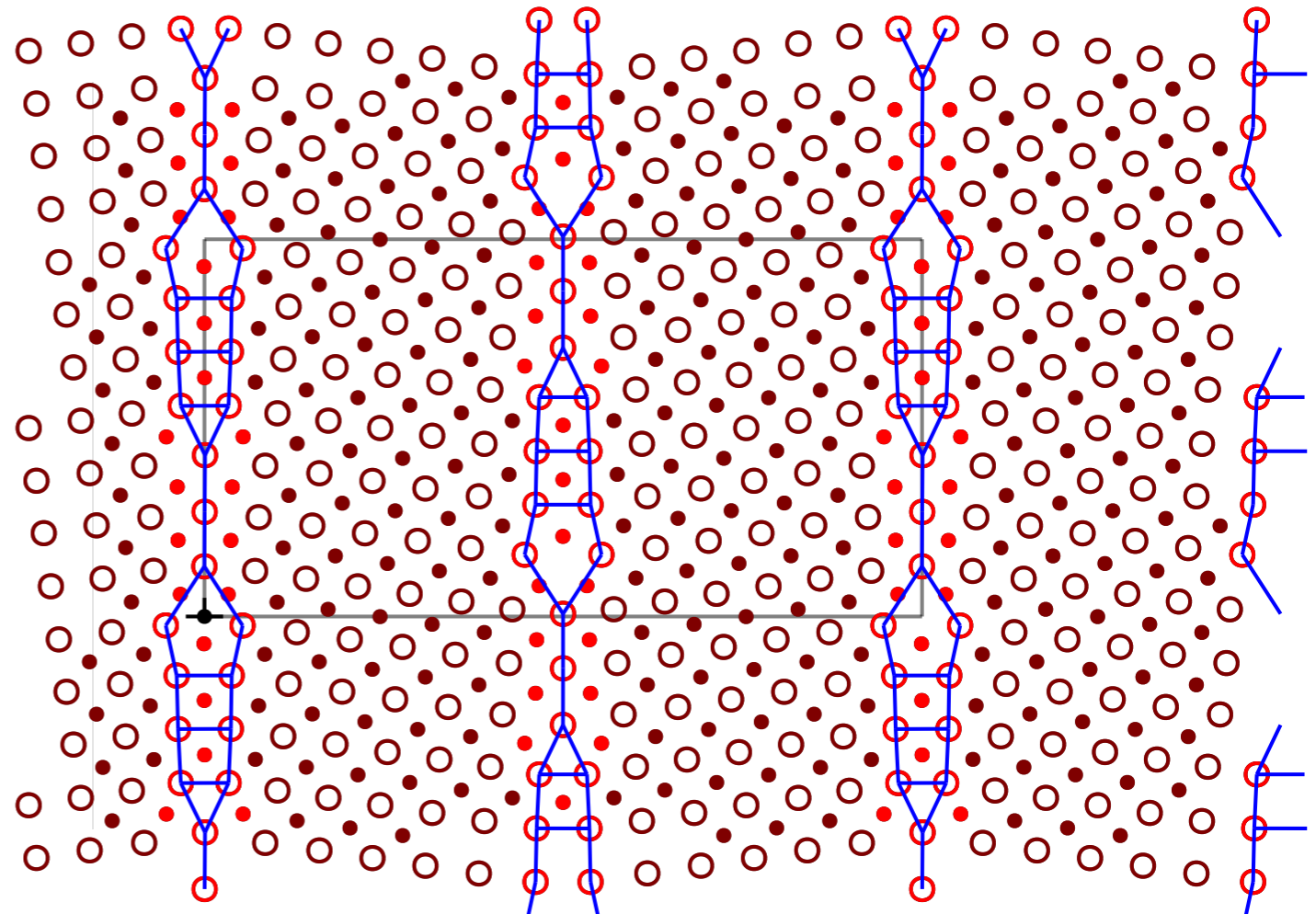
# EAM analysis

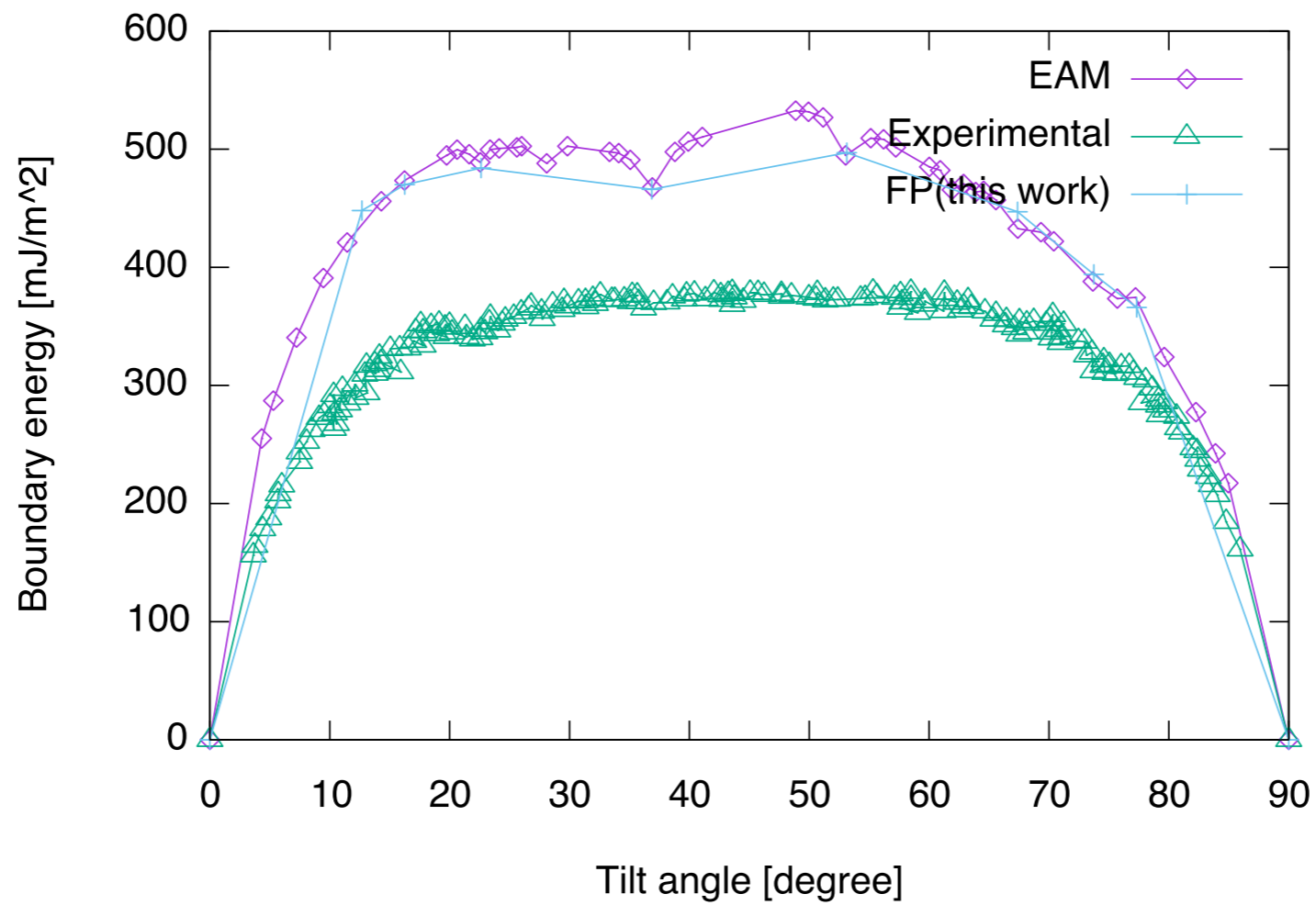
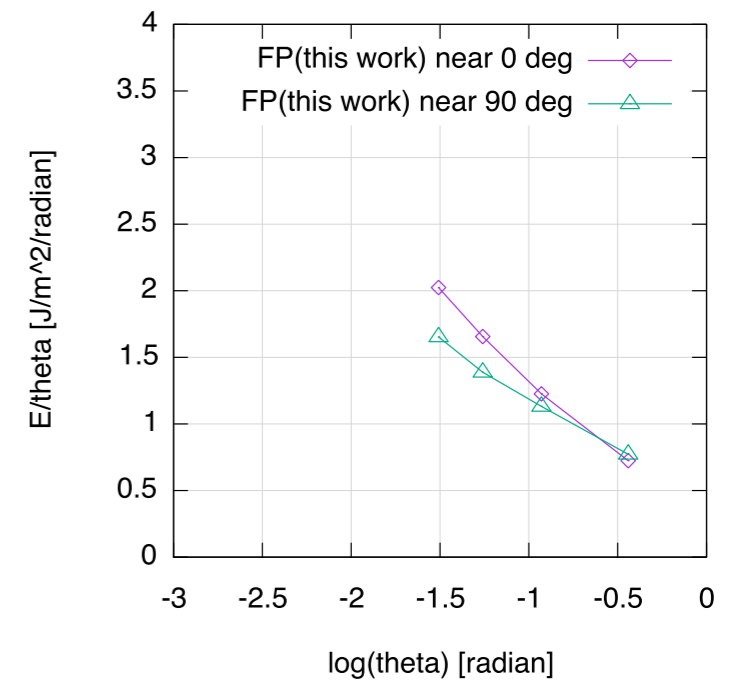
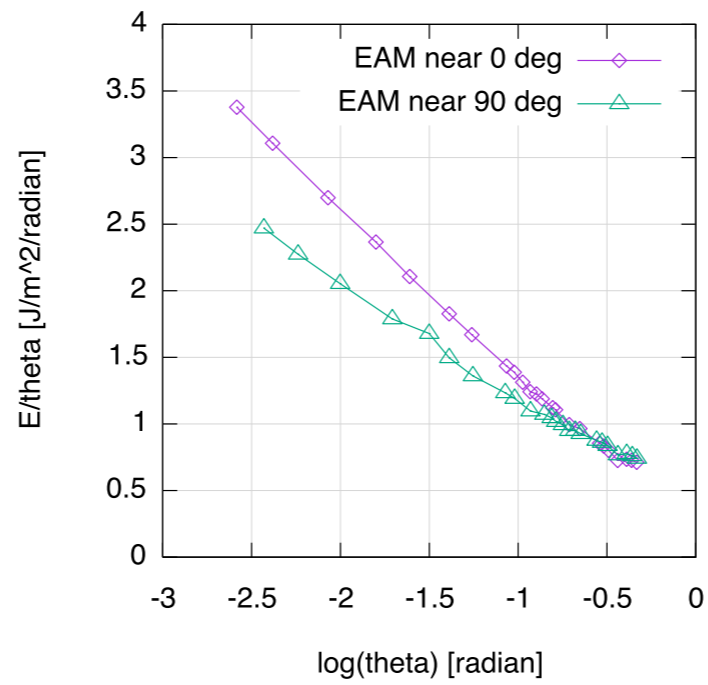
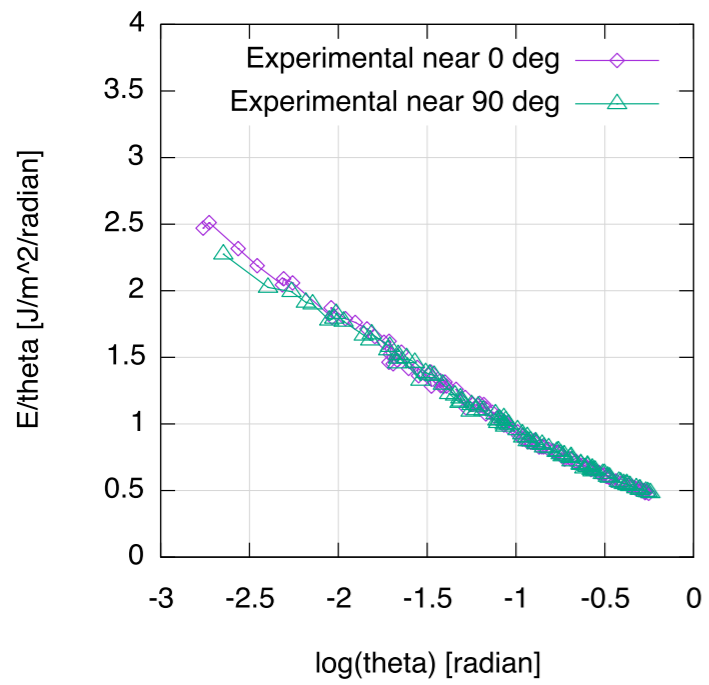


POSCAR\_0\_4417\_88\_-8\_0

## boundary structure

$$\theta = 16.26^\circ,$$
$$73.74^\circ$$





# VASP calculations for tilt boundaries

Cu



# VASP calc. conditions

Pseudo Potential: PAW-PBE

Relaxations: outer relax by hand

fix calc after relaxations

INCAR

Energy Cut off: 273.214eV

IBRION = 2 #Relax ions with conjugate-  
gradient

ISIF = 2 #Relax ions, calc stress

EDIFF = 1.0e-05

#criteria for electronic SC-loop

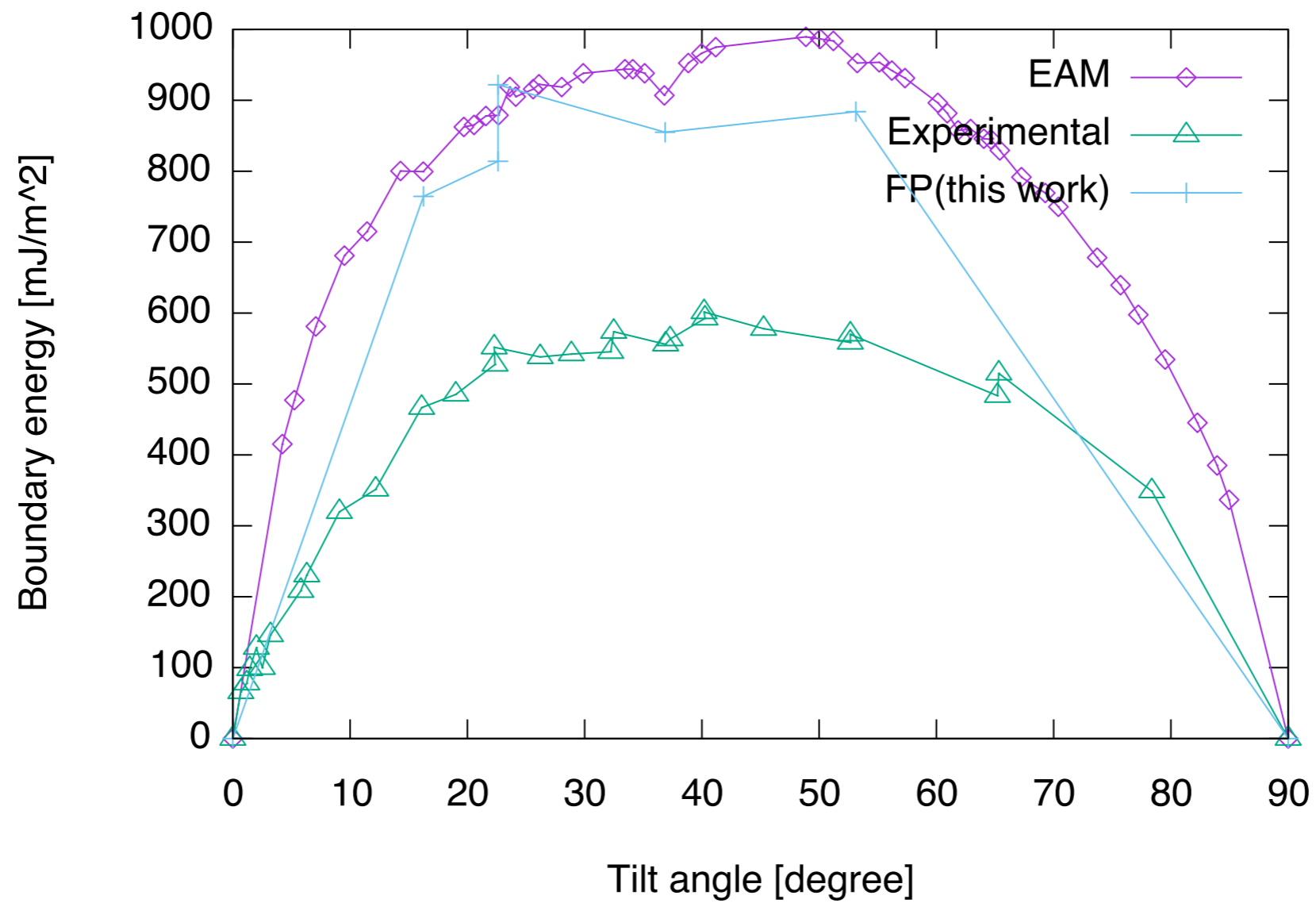
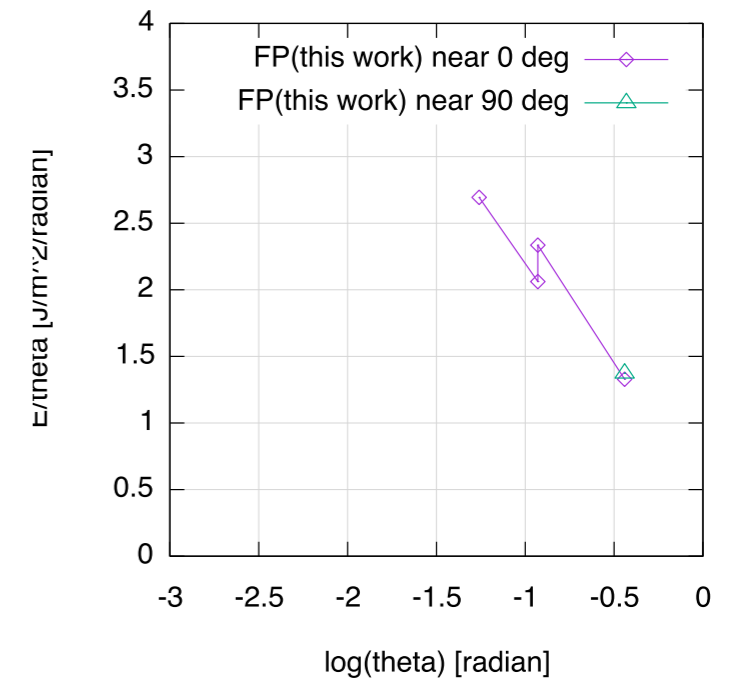
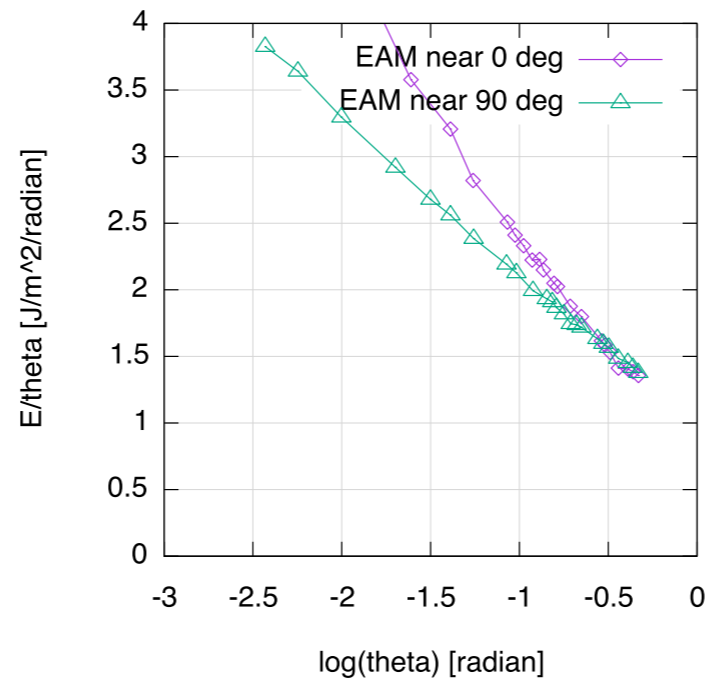
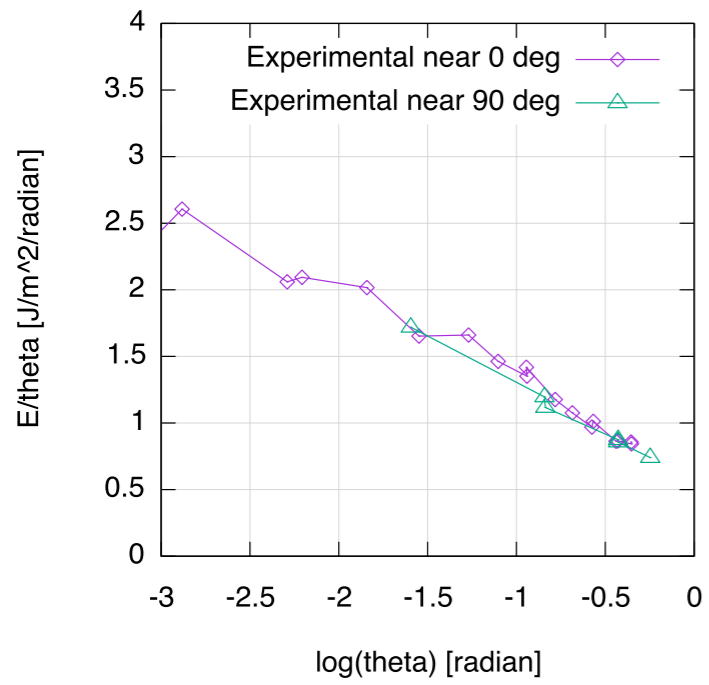
EDIFFG = -0.02

#criteria for ionic relaxation loop

KPOINT

Use automatic

length=100 due to d-electron



EAM analysis:  
local energy,  
strain field

# local energy

- local energy and force from the first principles

- Under construction by M. Kohyama(AIST),  
Y. Shiihara(Tokyo->Toyota-TI)

- R Kobayashi(Nagoya TI)

- using a fitted EAM potential

- first nearest neighbor

$$E_i = A \sum_j \exp(-p r_{ij}) - \sqrt{\rho}$$

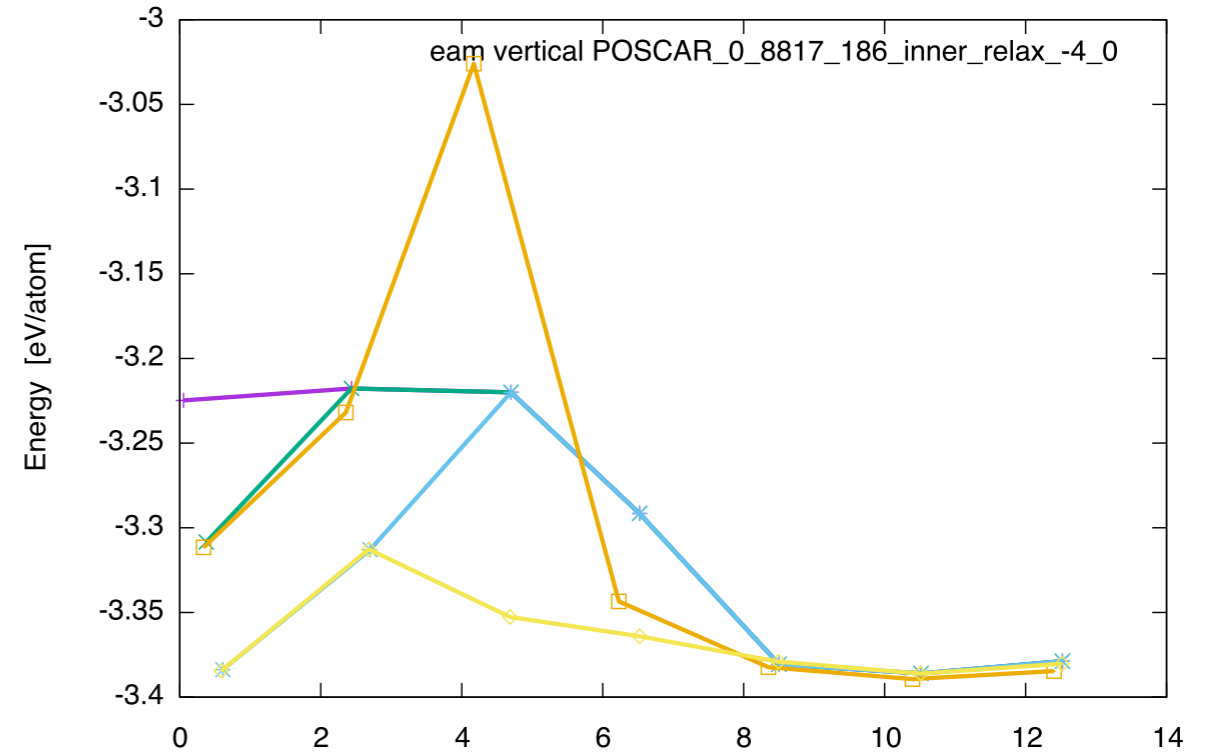
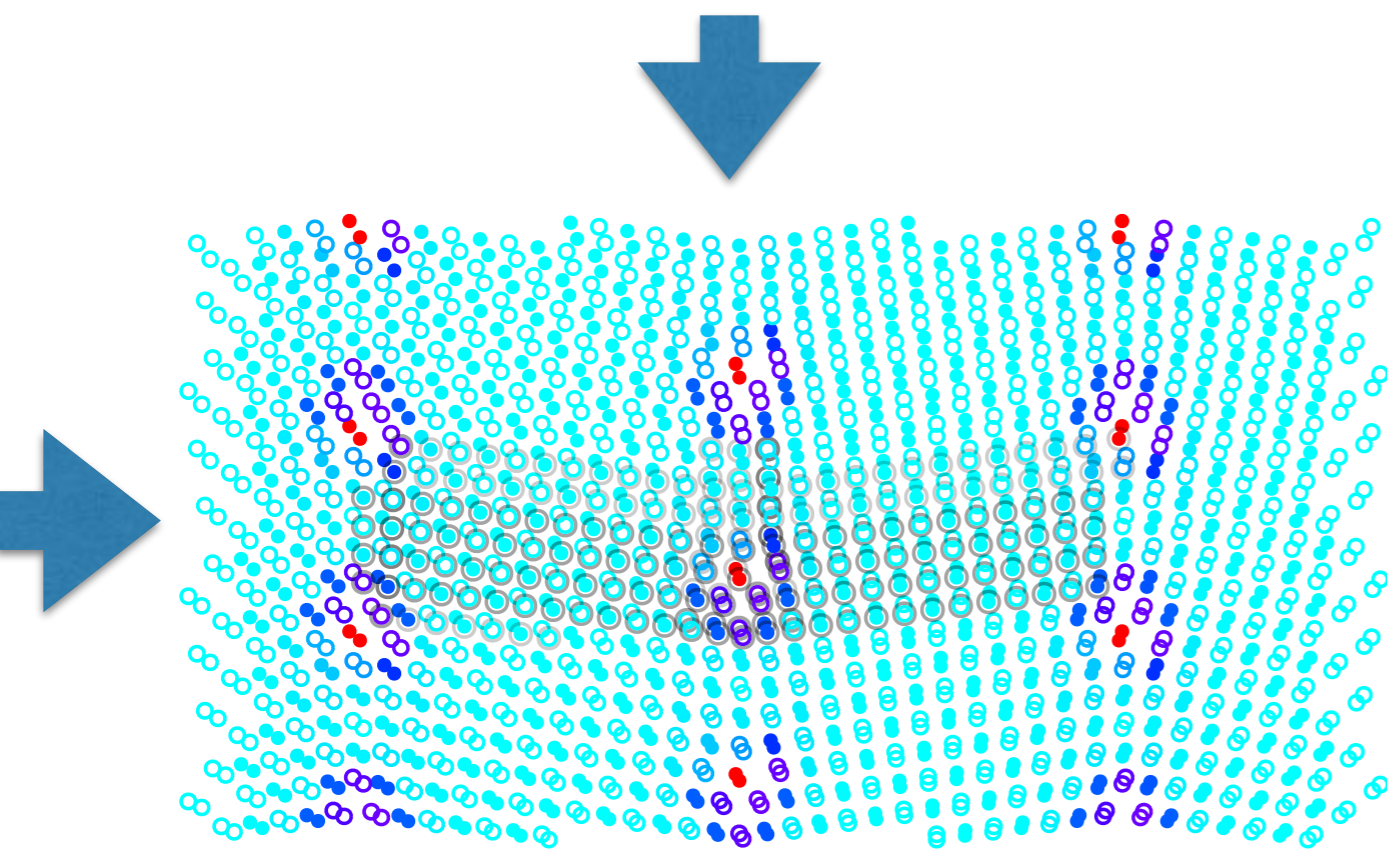
- Cohesive energy(3.39eV)

- equilibrium distance(r0)

$$\rho = \sum_j \{B \exp(-q r_{ij})\}^2$$

- vacancy  
formation energy(0.8eV)

- p=3.0 at r0



POSCAR\_0\_8817\_186\_-4\_0

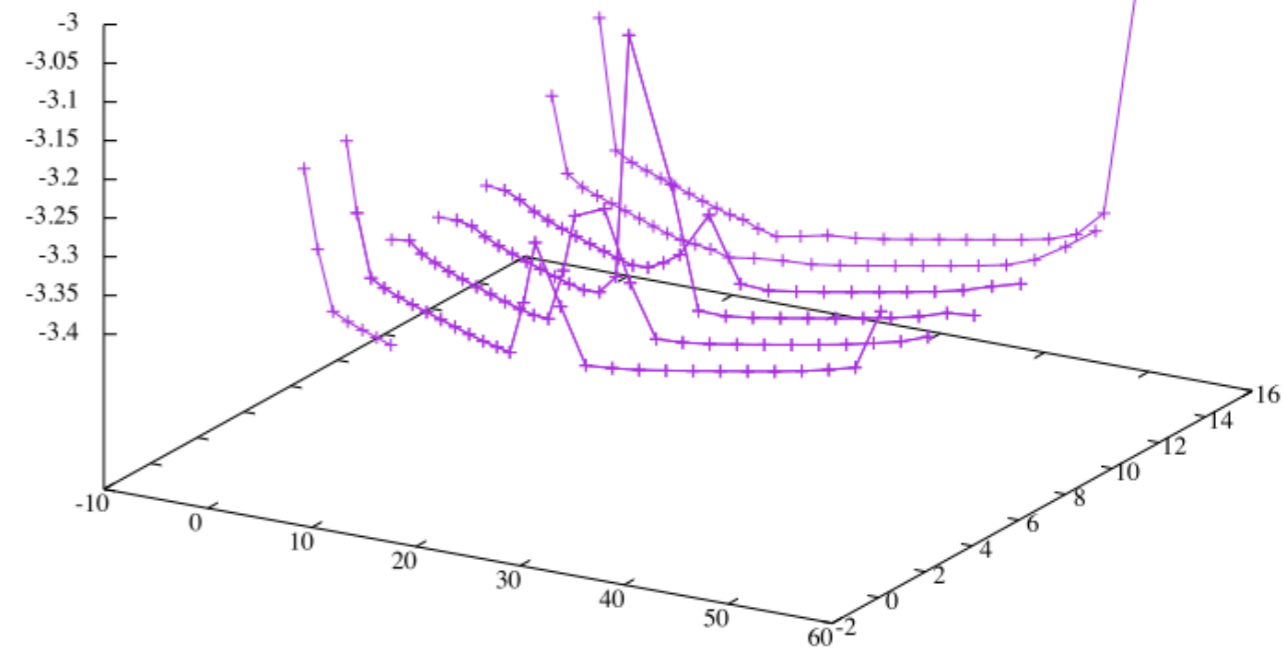
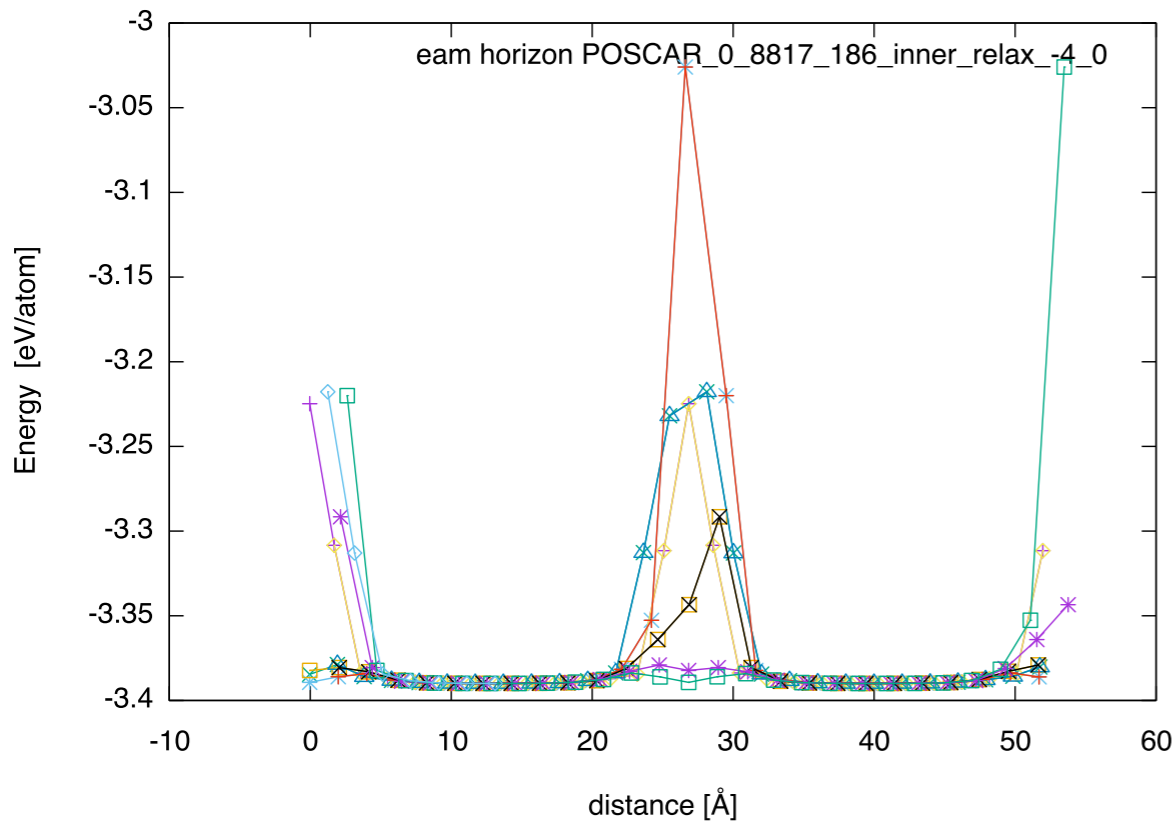
min\_e = -3.3900 [eV]

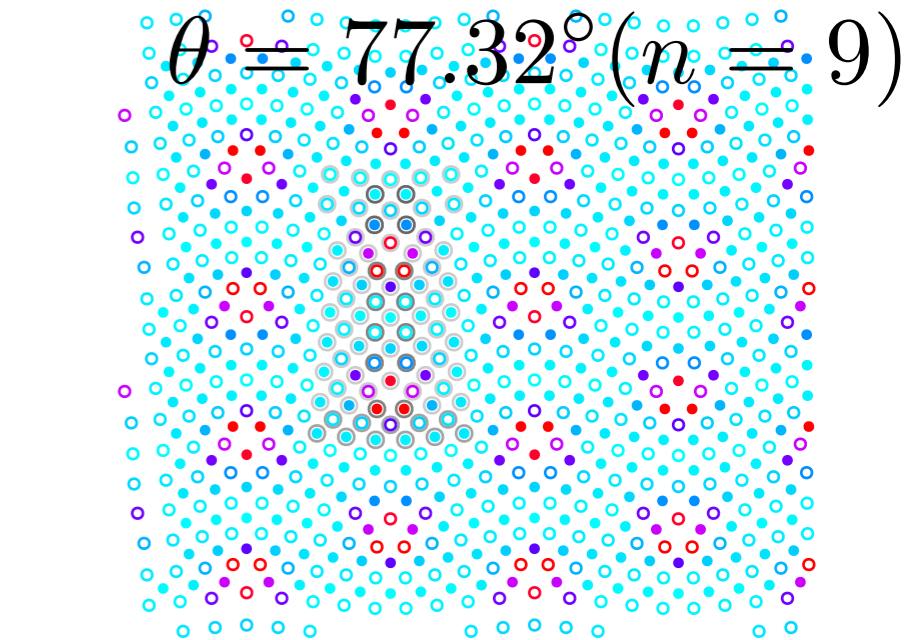
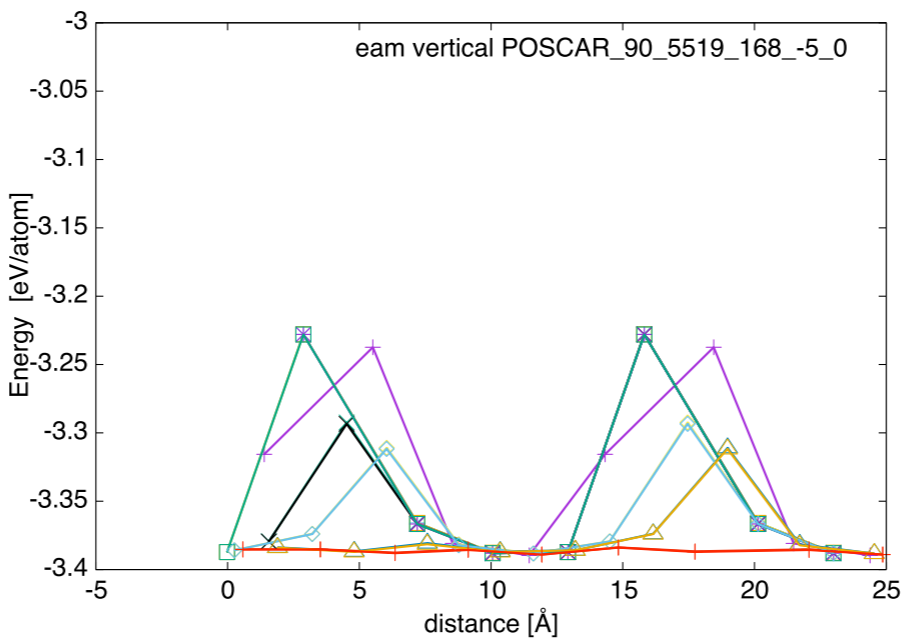
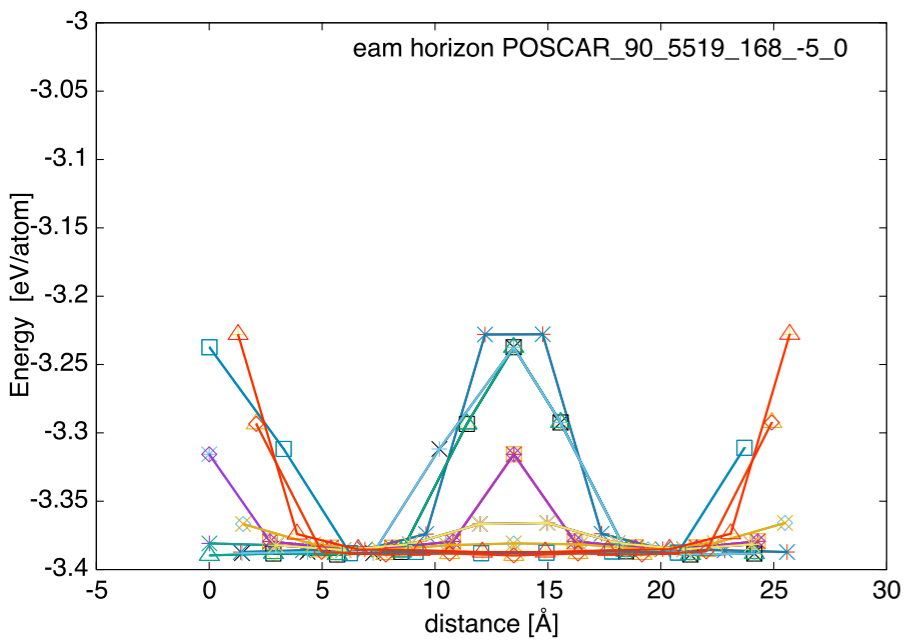
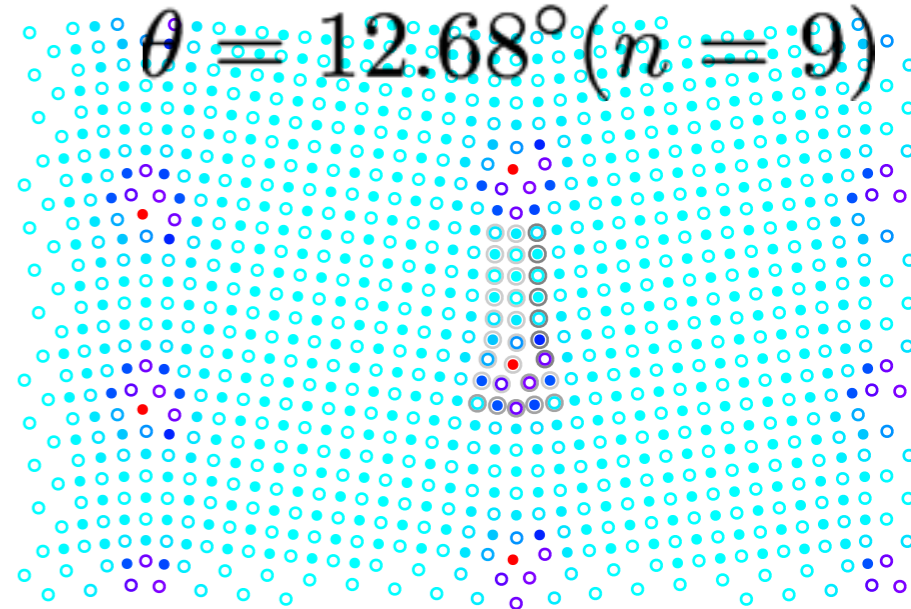
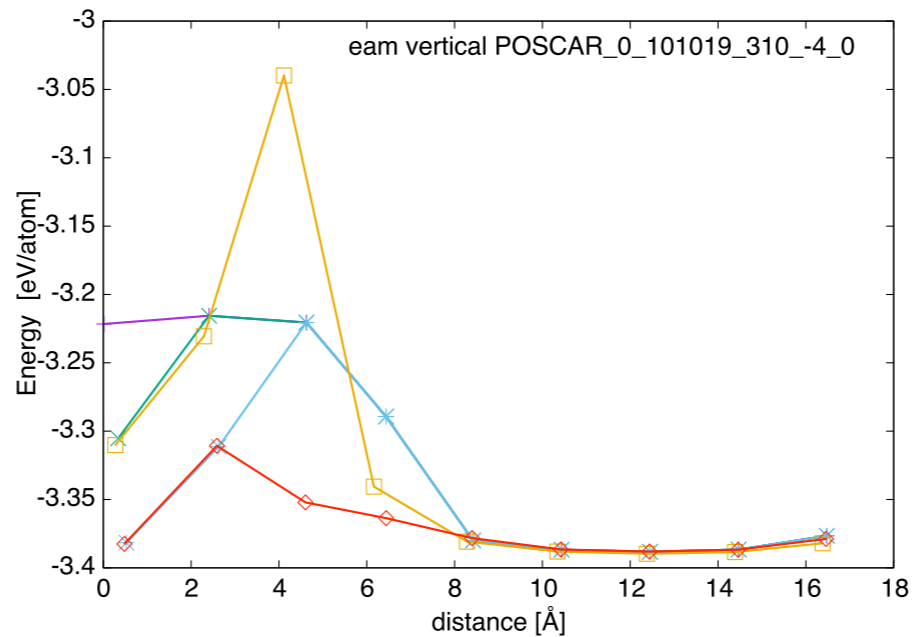
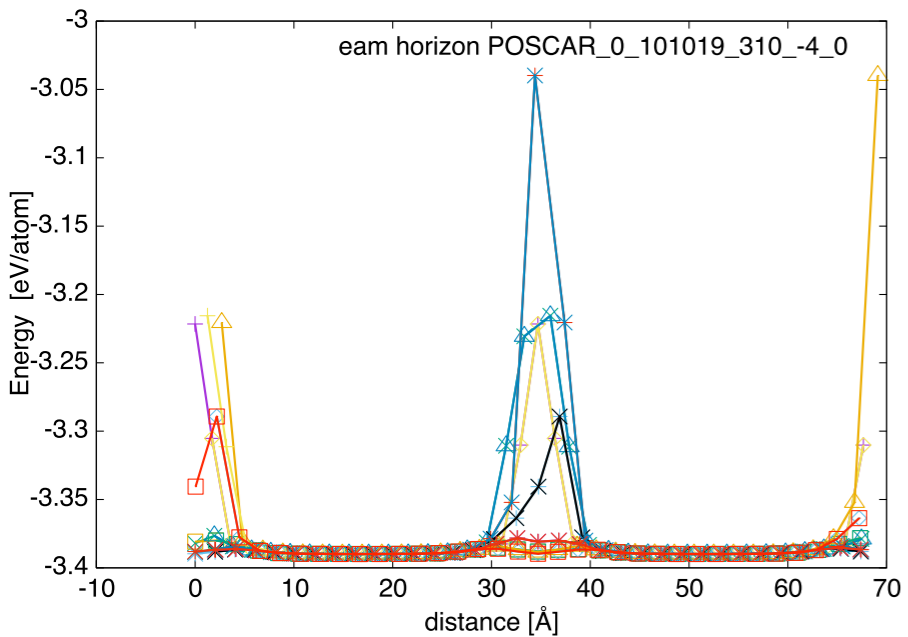
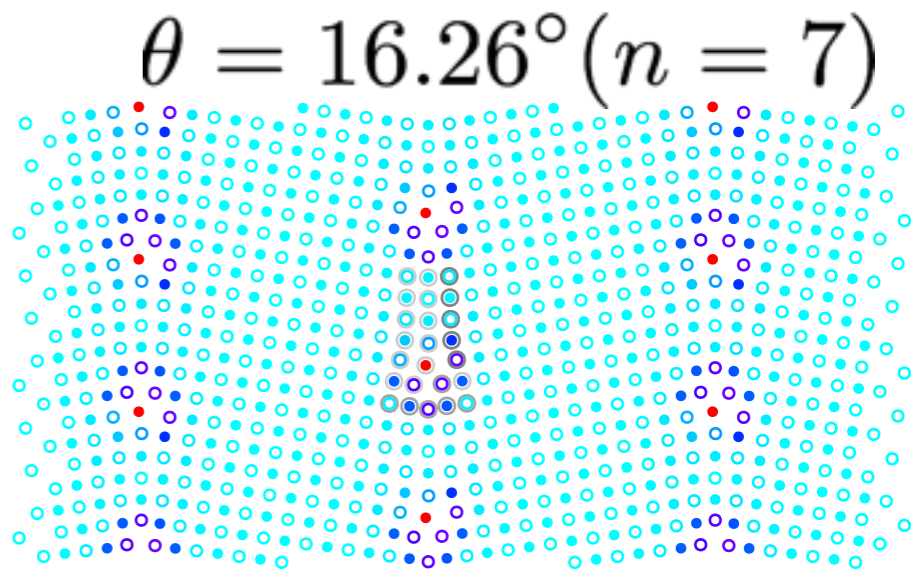
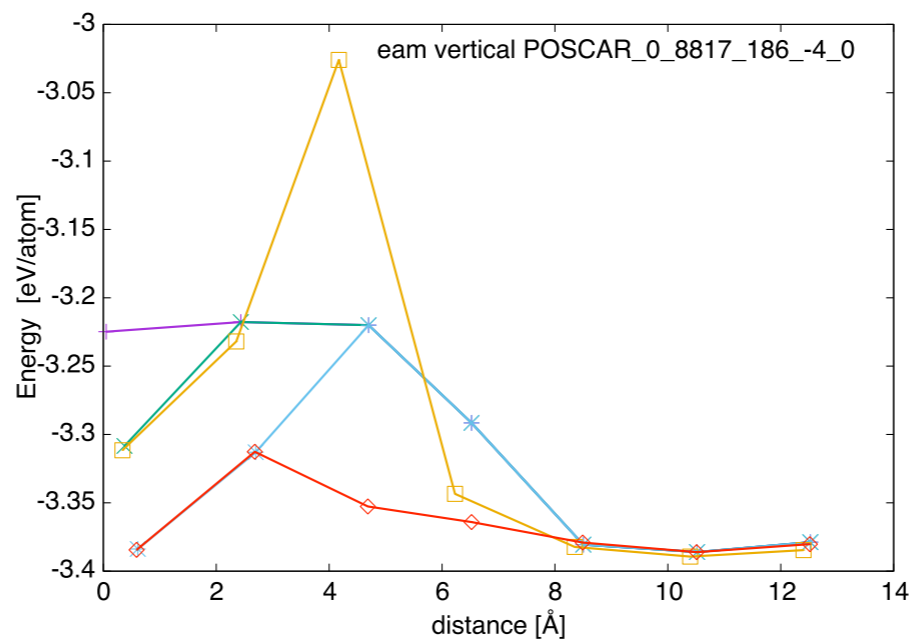
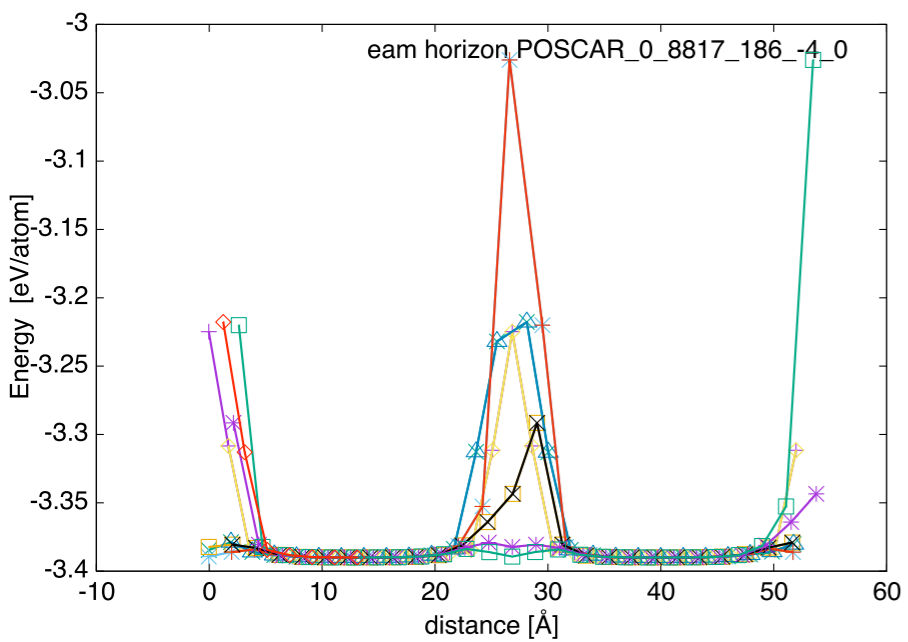
max\_e = -3.0260 [eV]

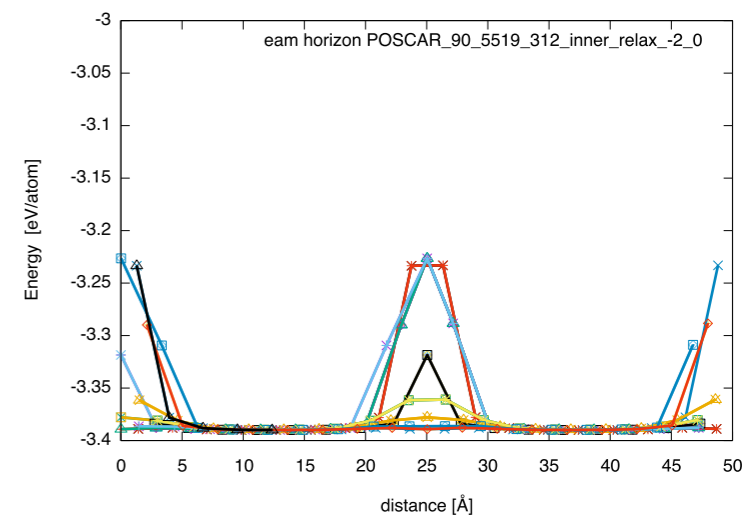
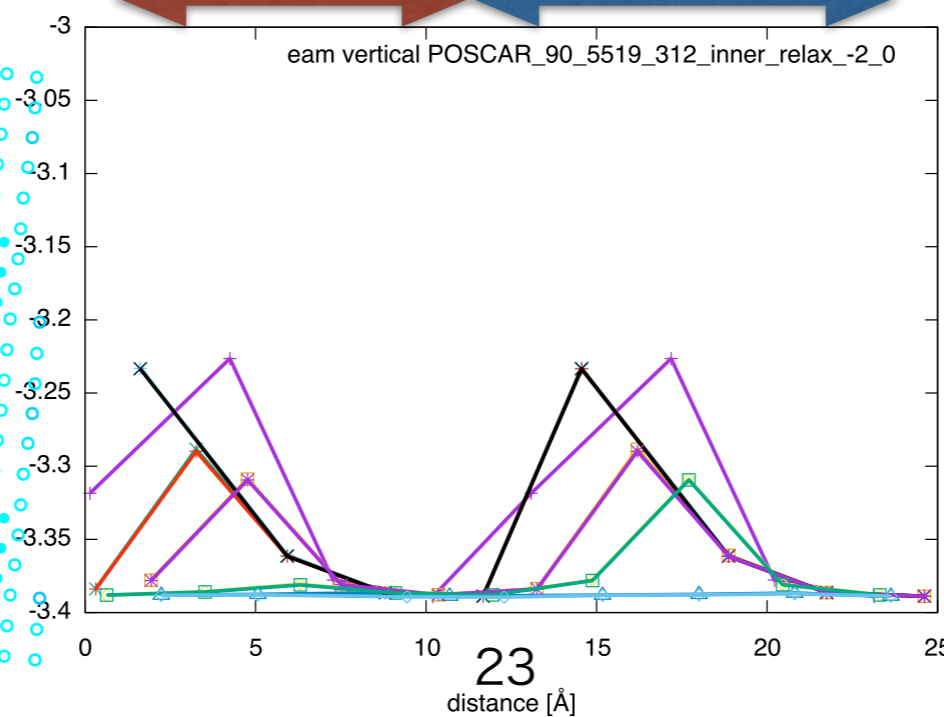
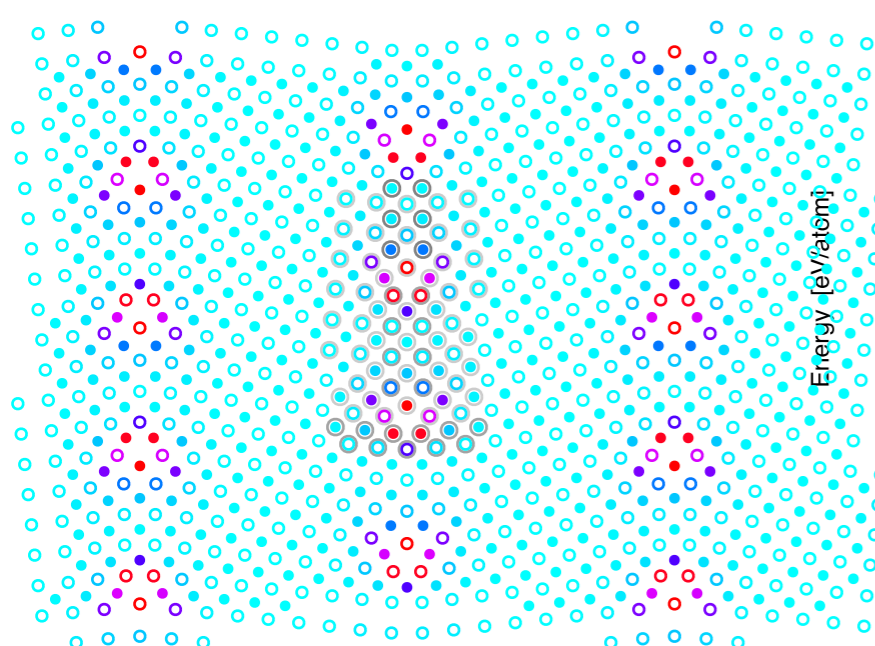
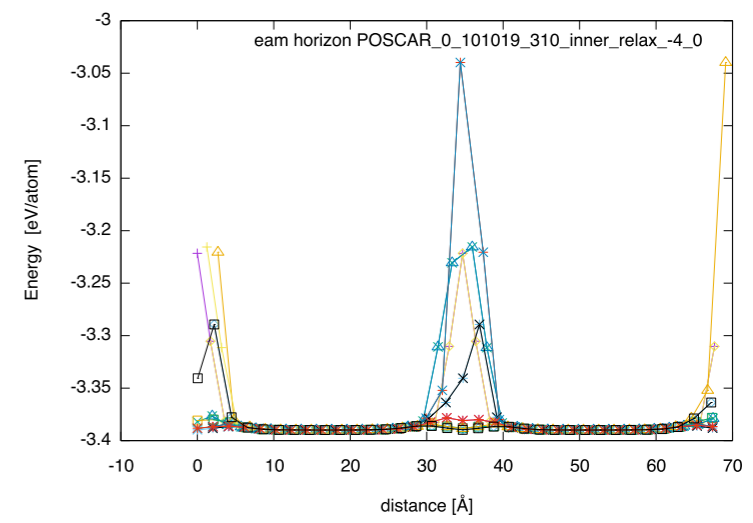
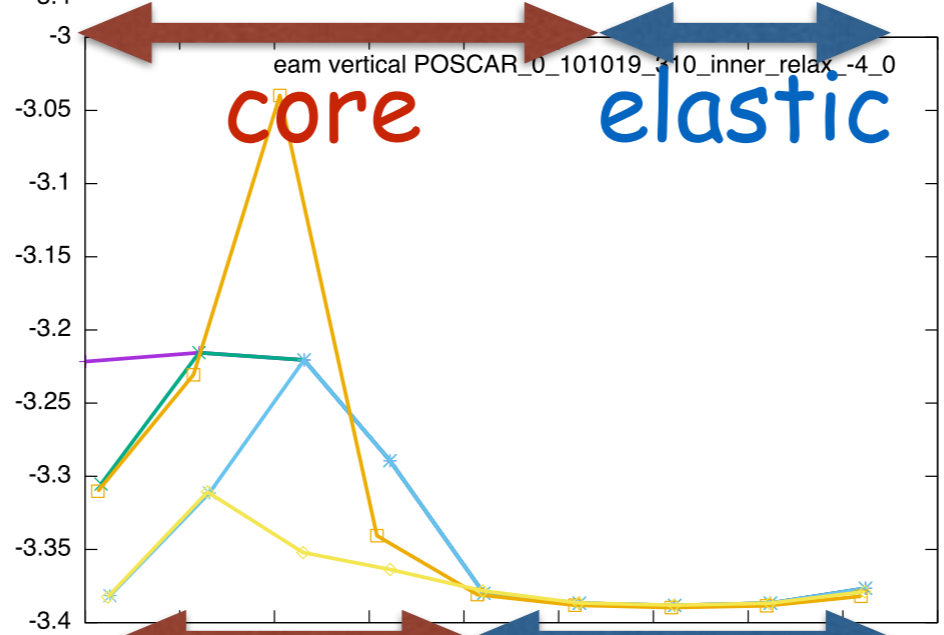
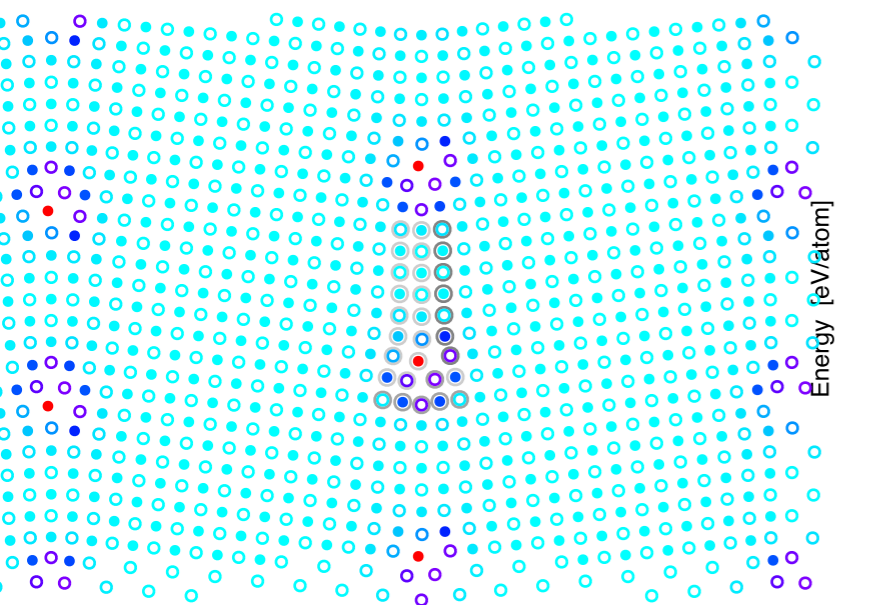
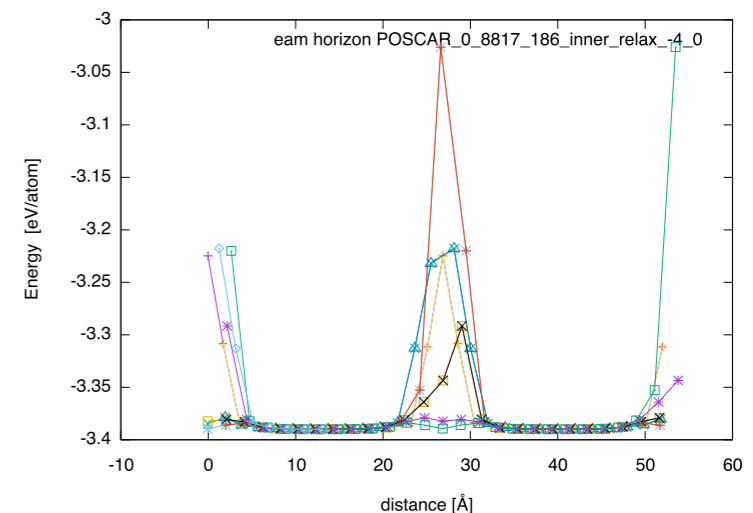
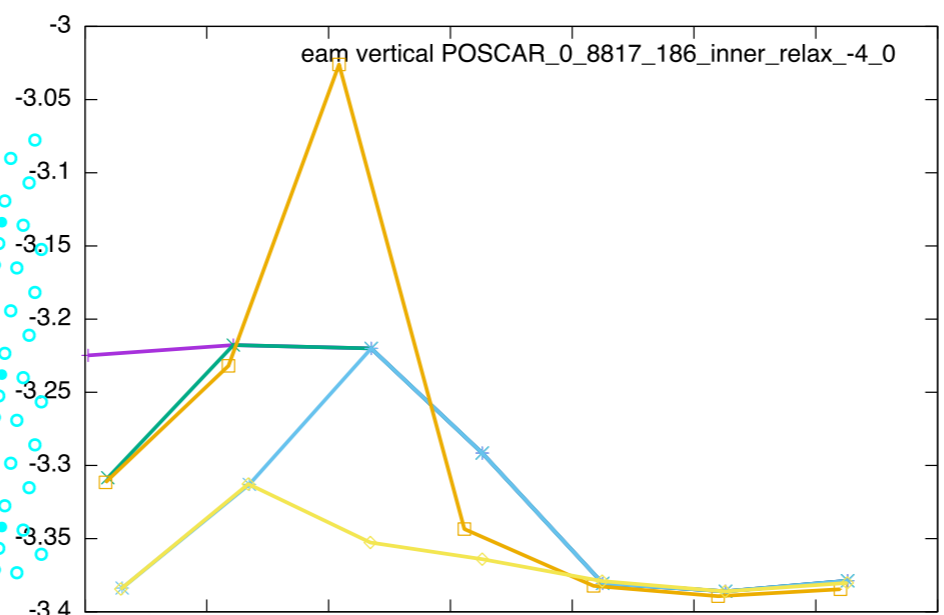
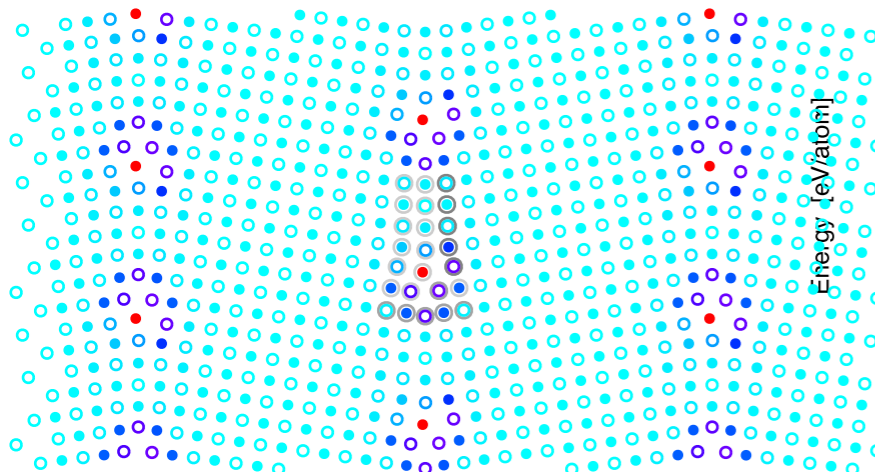
423 [mJ/m<sup>2</sup>]

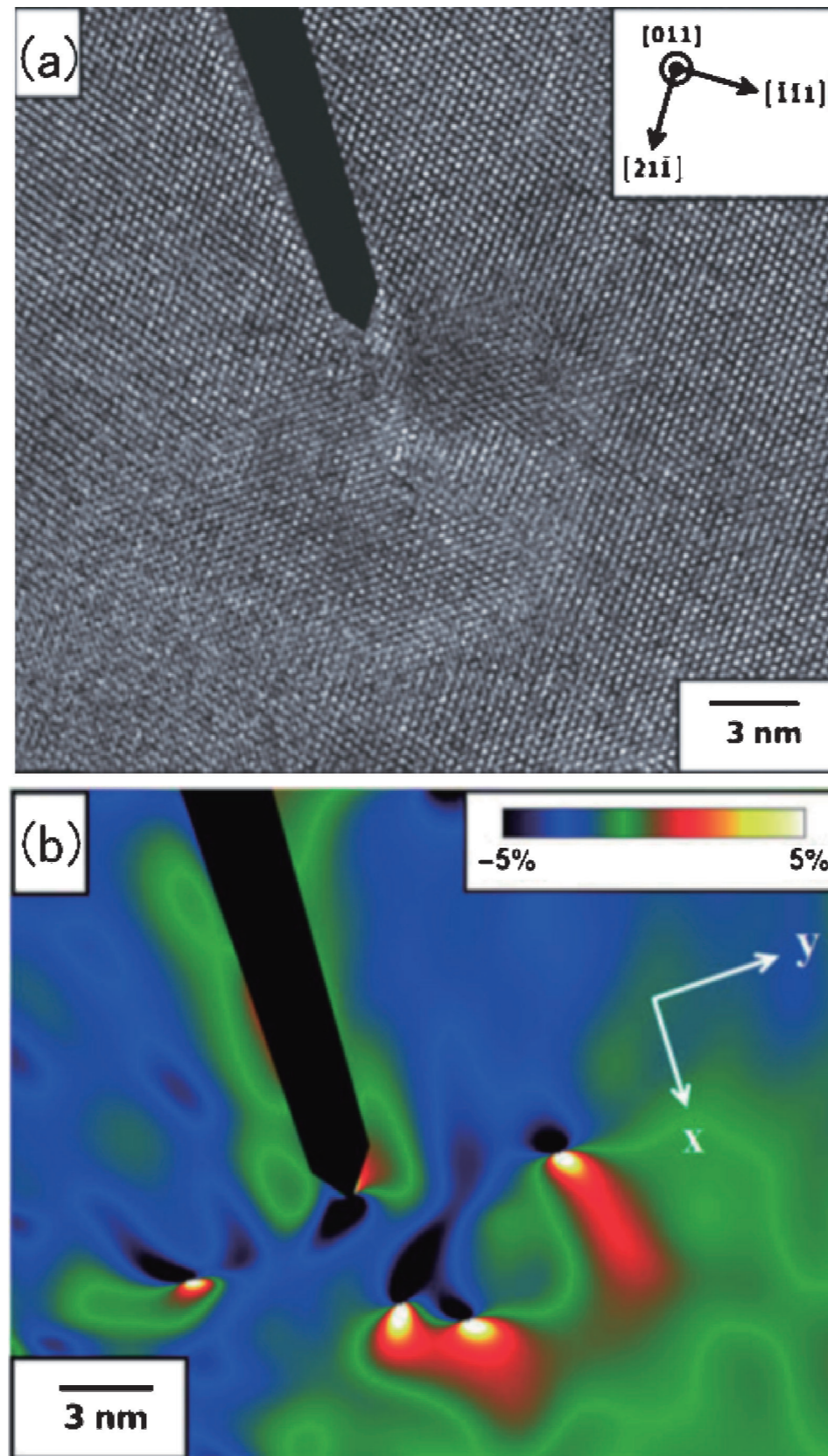
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x= -3.701, y= -0.211 || 419



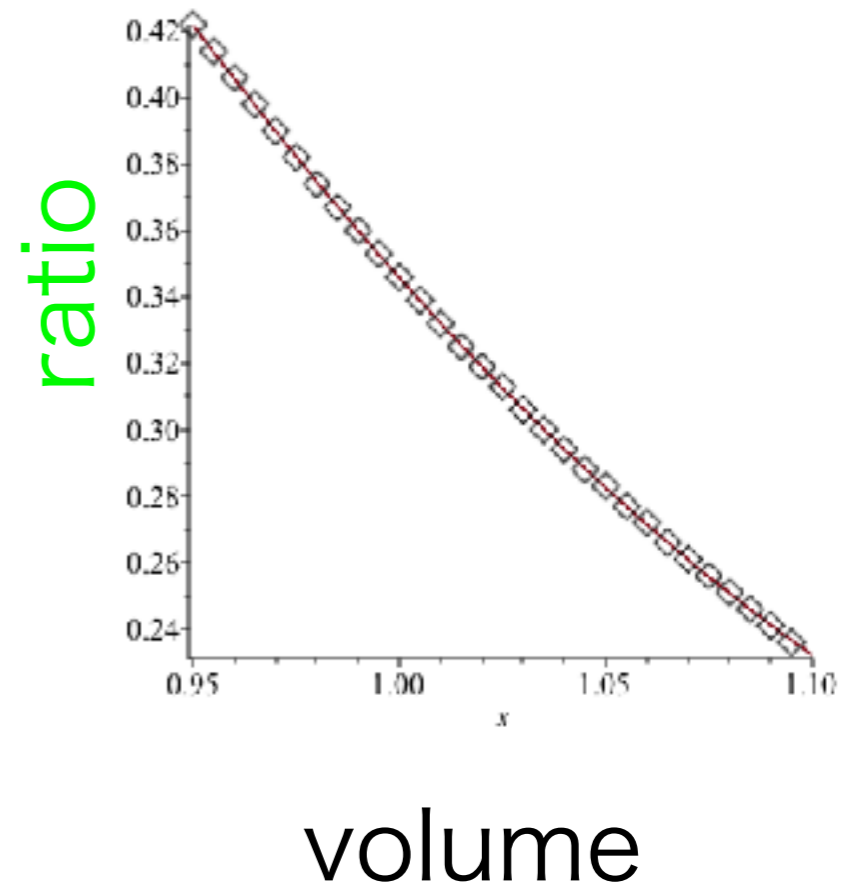
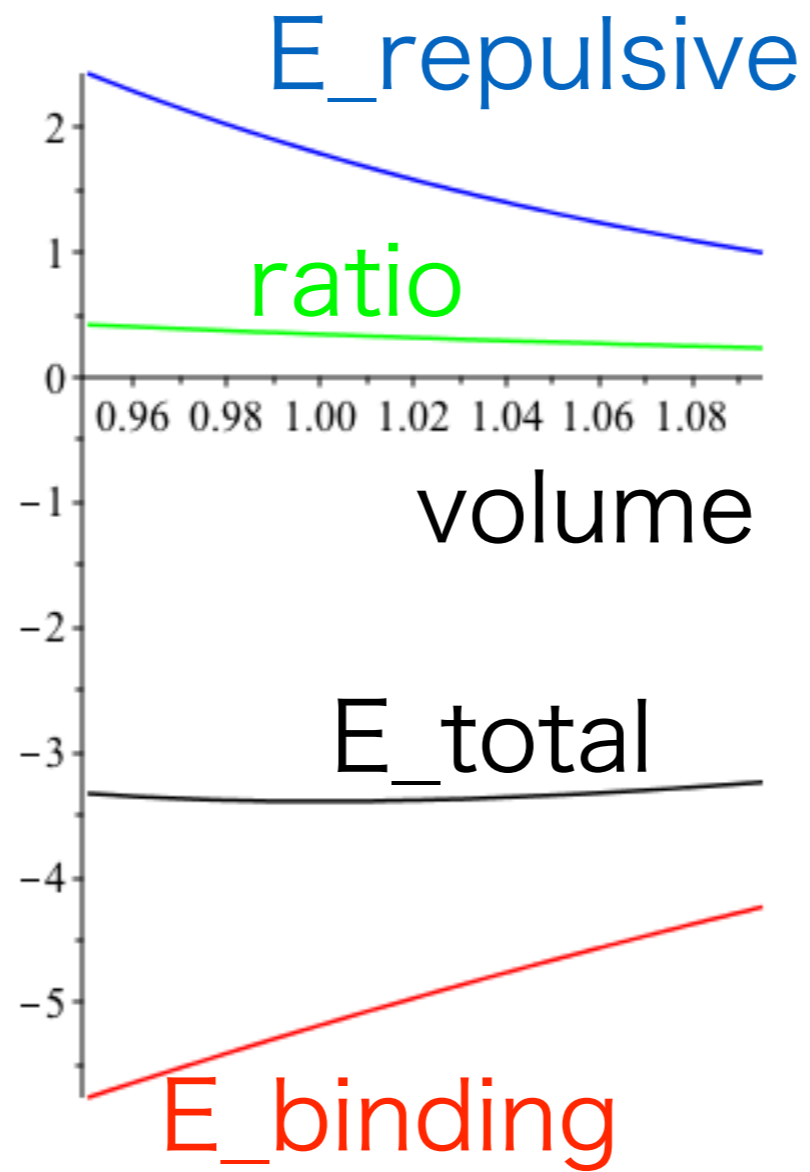
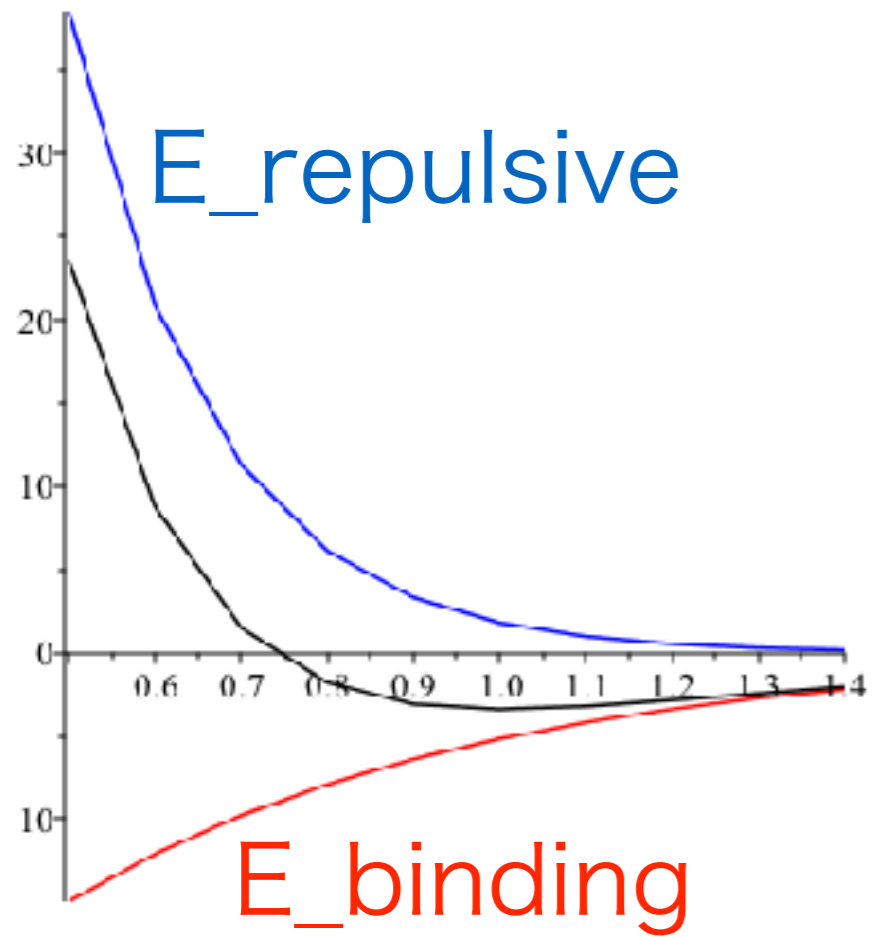






GPA(geometrical phase analysis)により表示された可視化クラック先端の歪場。  
「亀裂先端転位と脆性 延性遷移挙動」, 田中將己 定松直 東田賢二, まてりあ, 56 卷  
(2017) 10 号 p. 597-603.





$$E_i = E_{\text{repulsive}} + E_{\text{binding}}$$

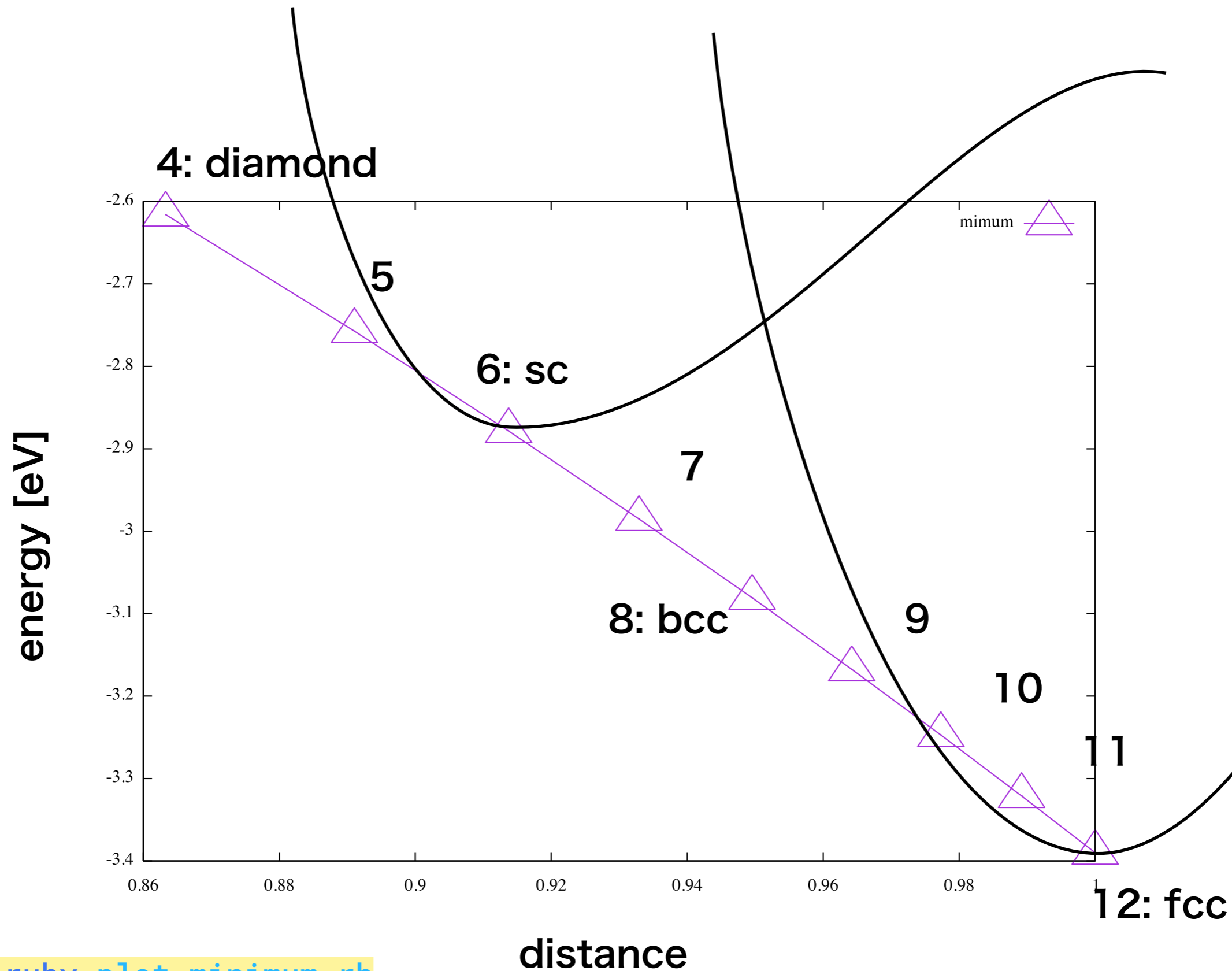
$$= \sum_j \phi(r_{ij}) - \sqrt{\sum_j h(r_{ij})^2}$$

$$\phi(r_{ij}) = A_0 \exp(-pr_{ij})$$

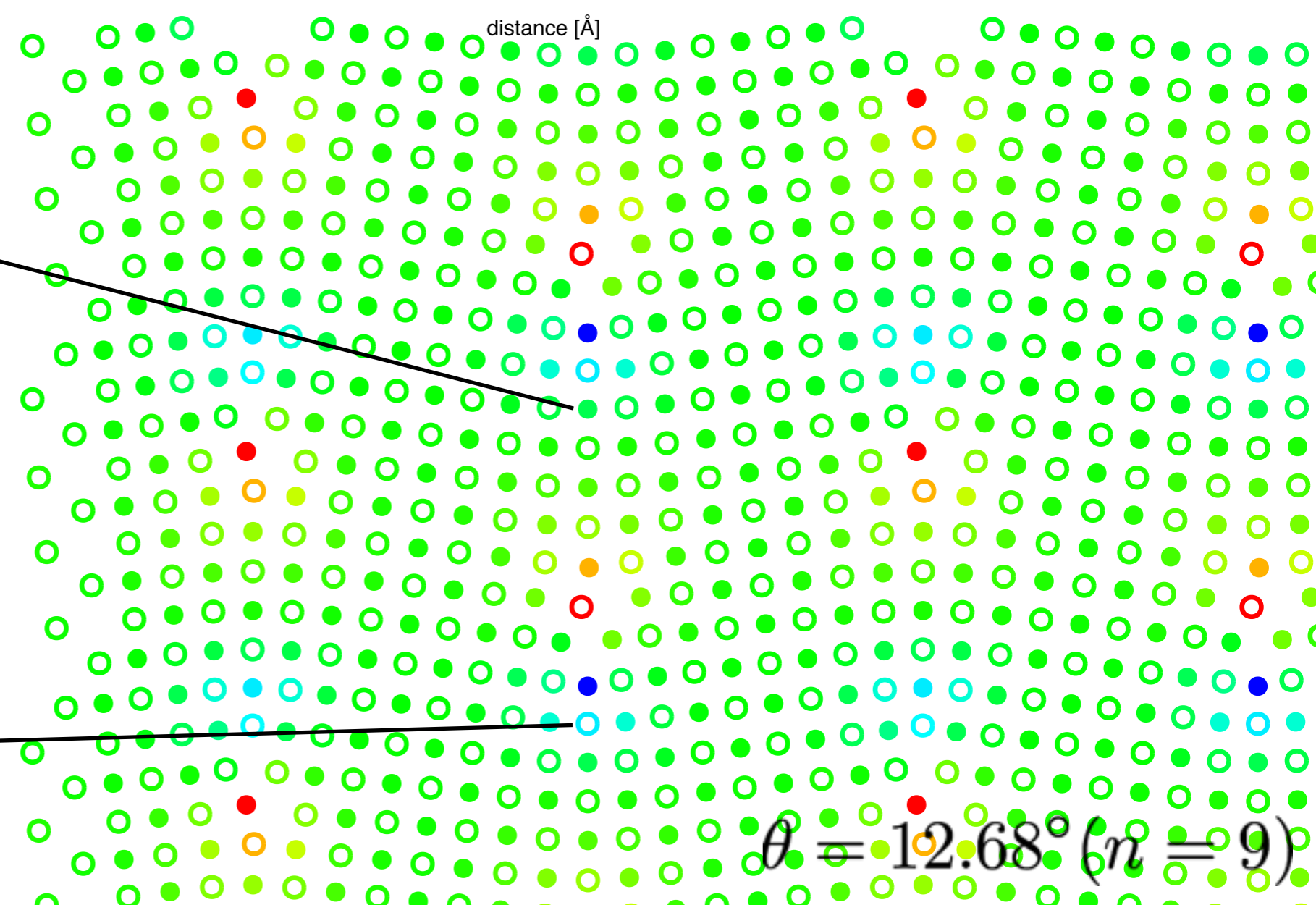
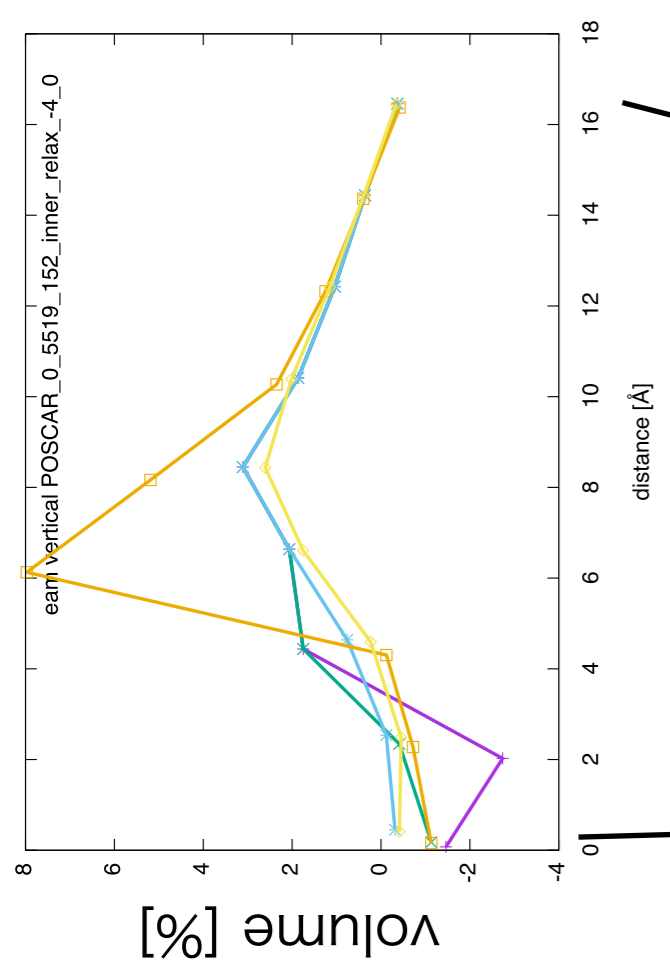
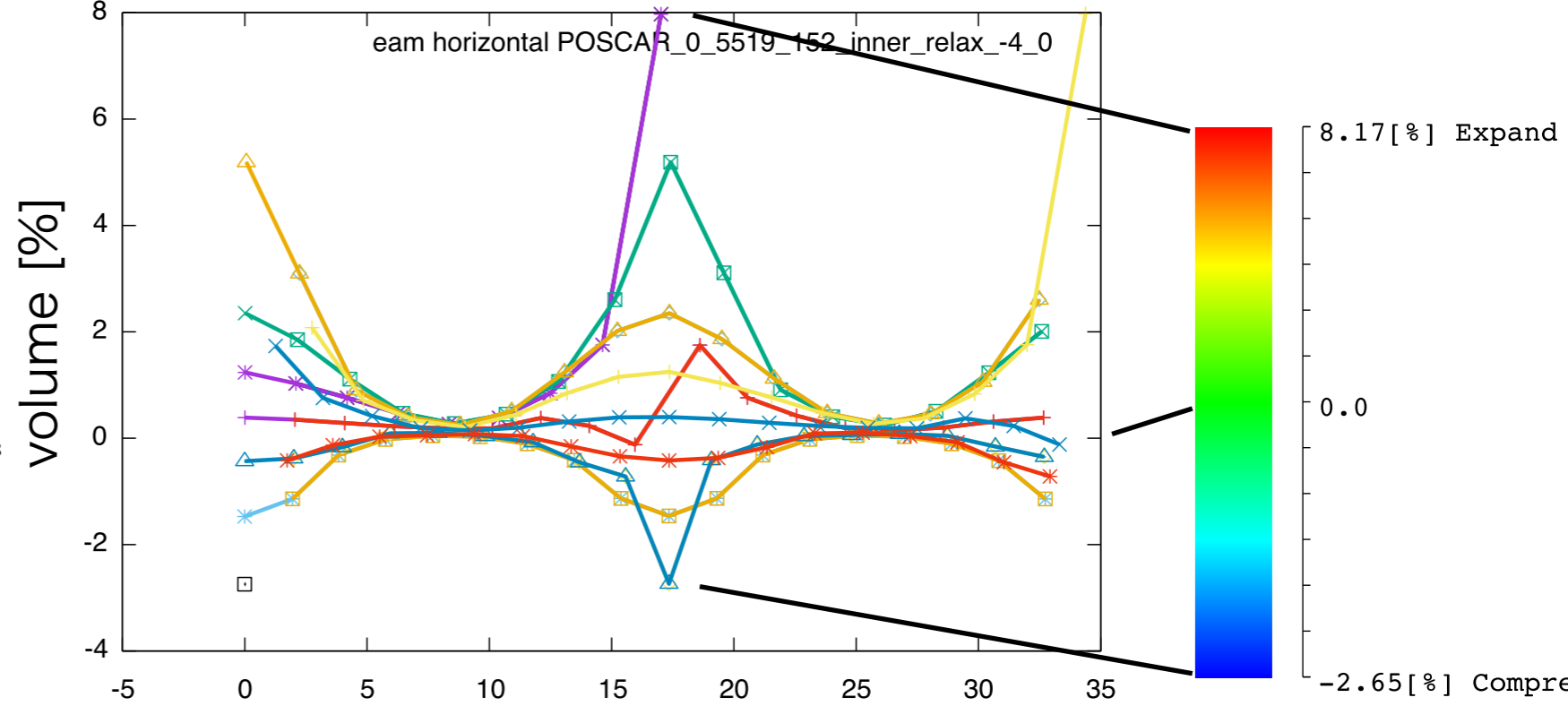
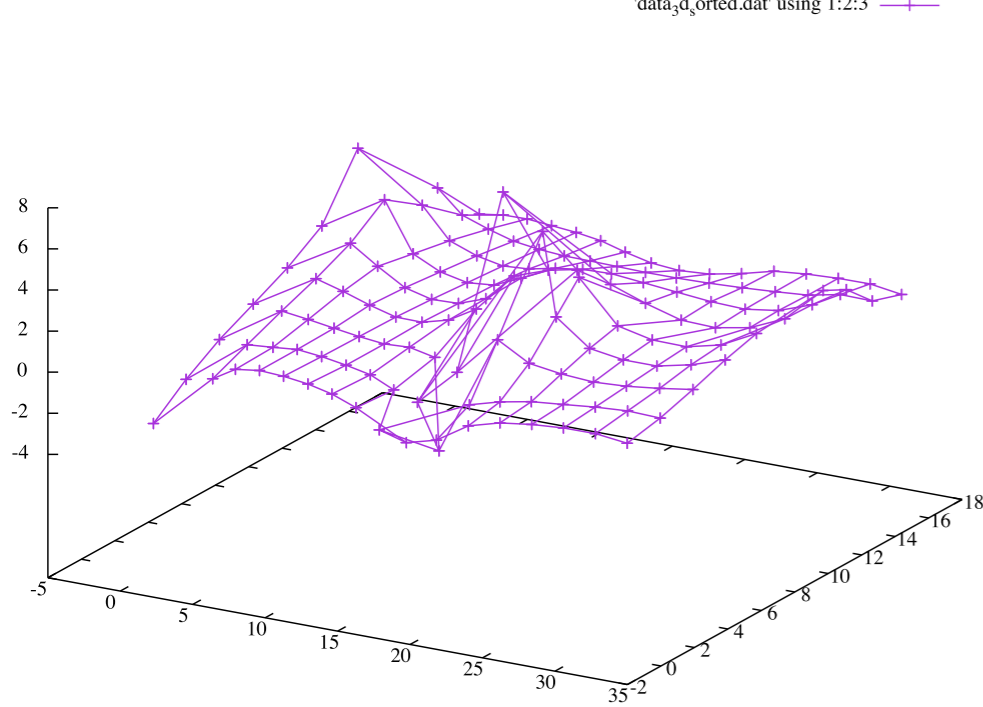
$$h(r_{ij}) = B_0 \exp(-qr_{ij})$$

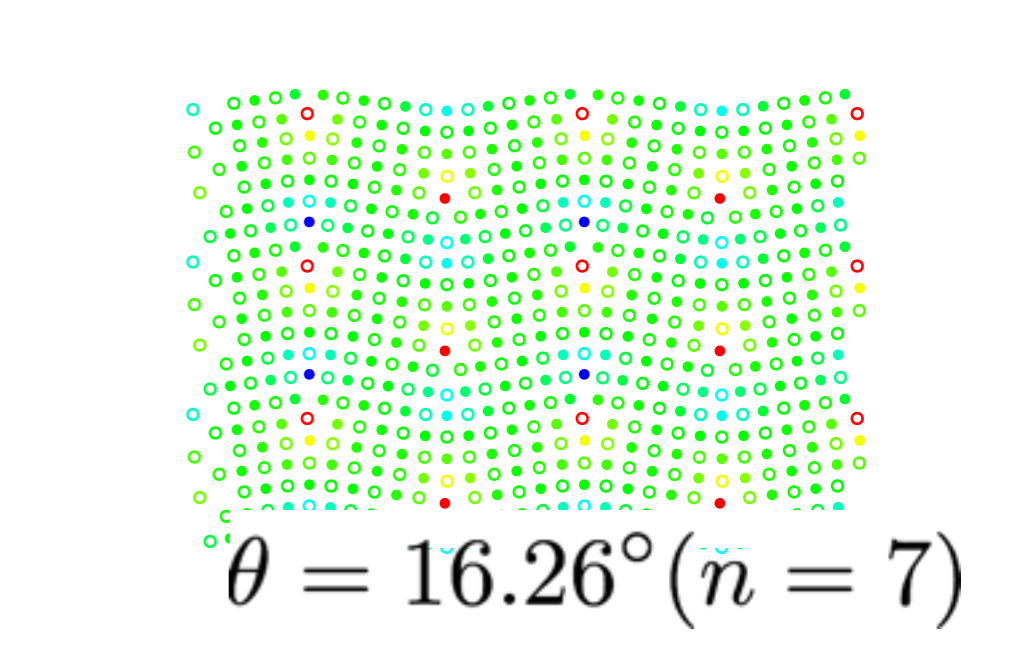
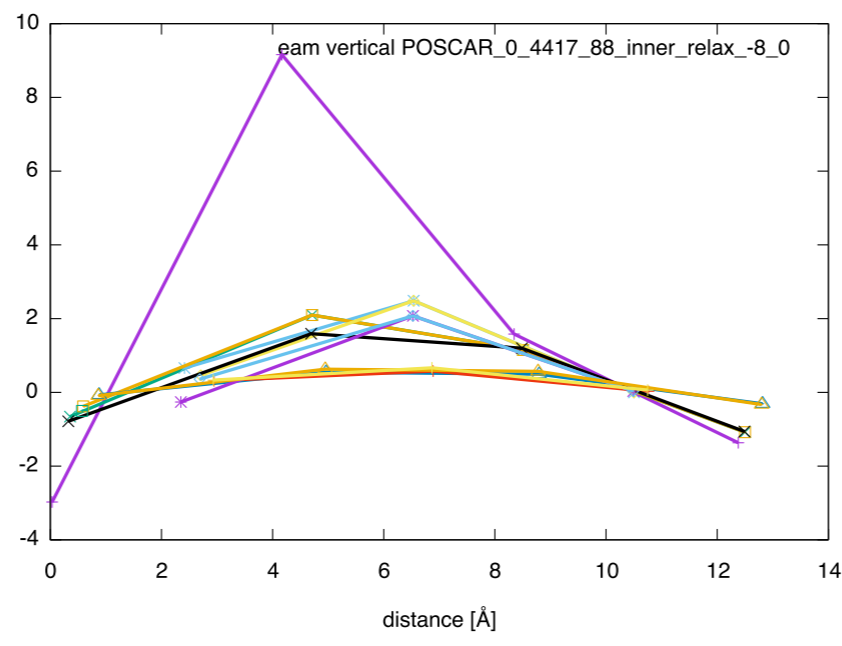
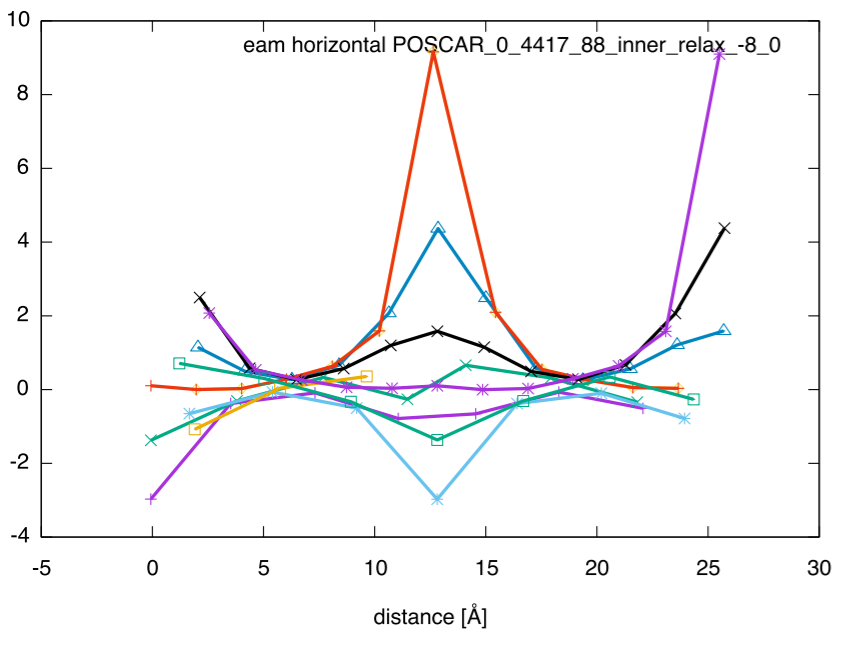
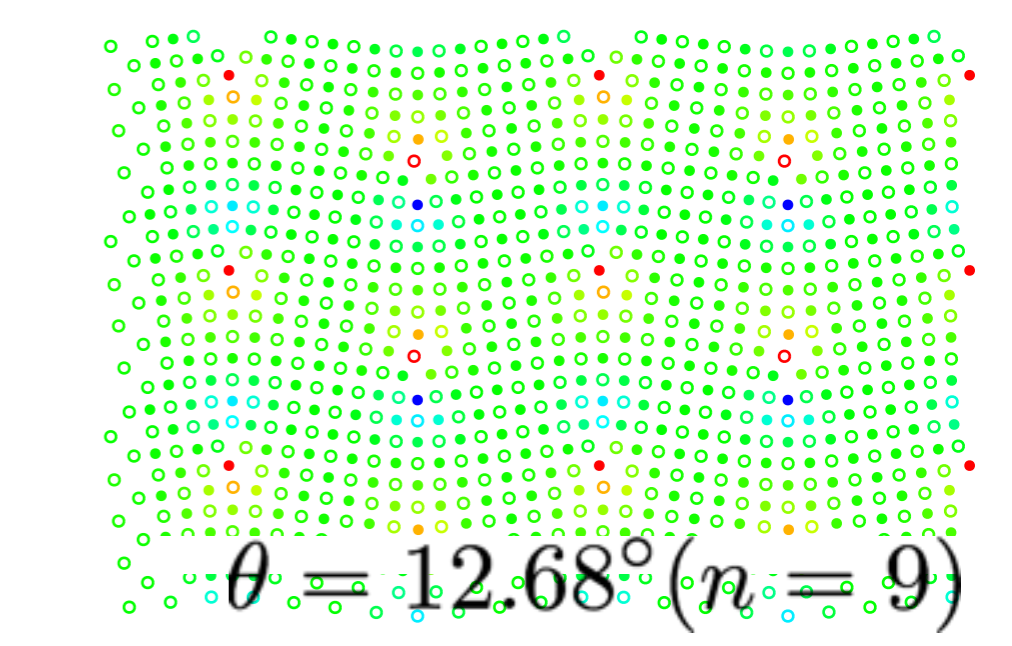
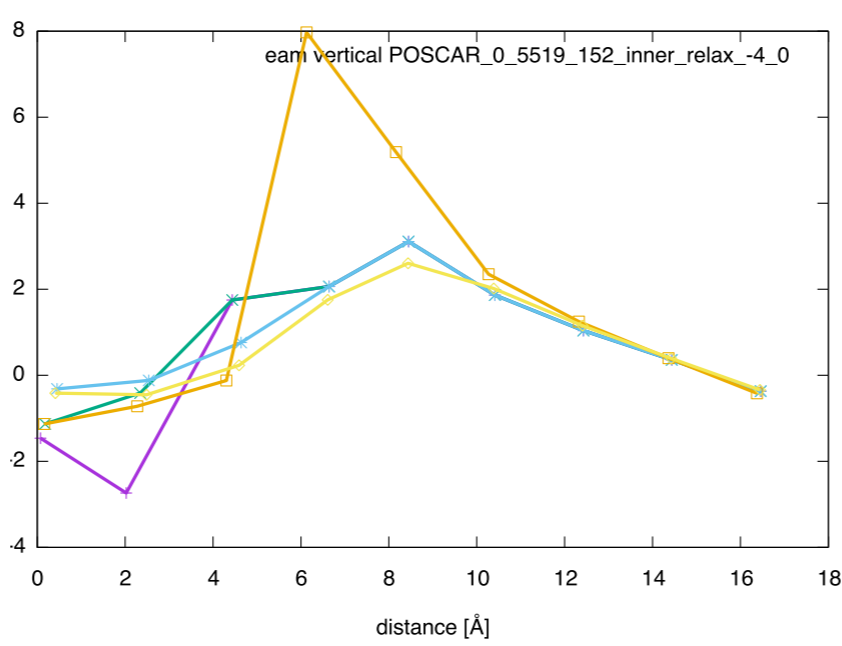
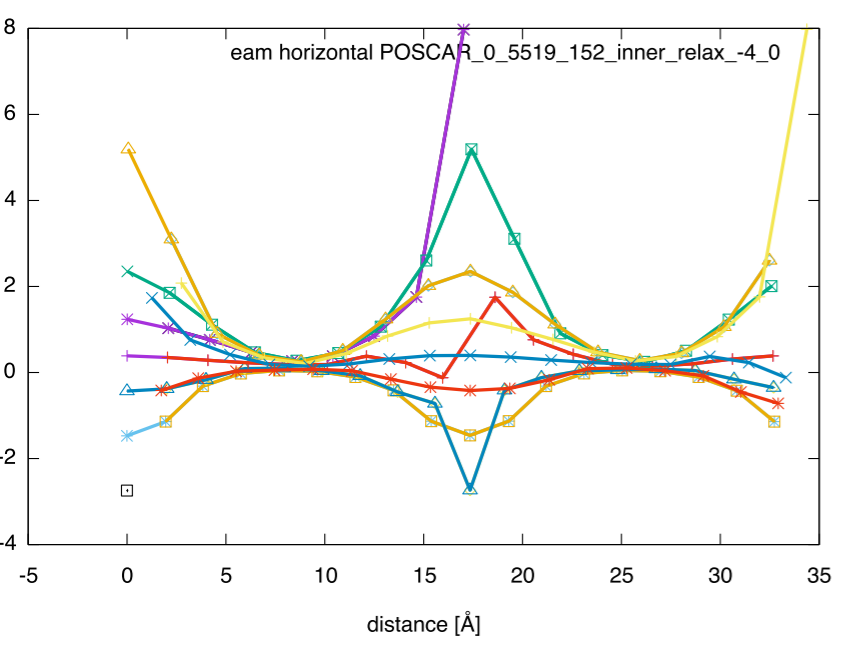
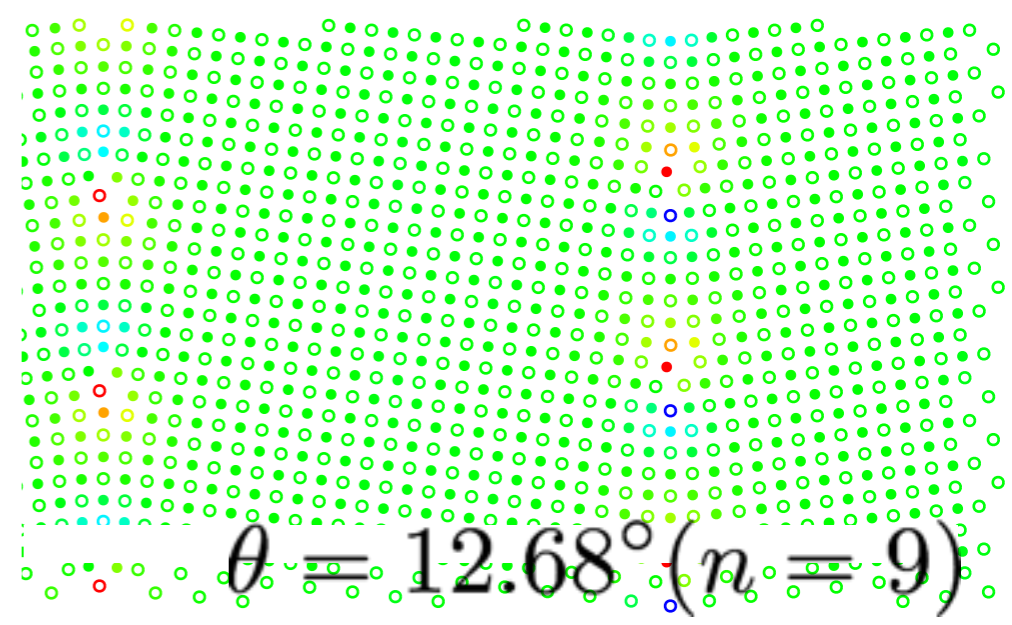
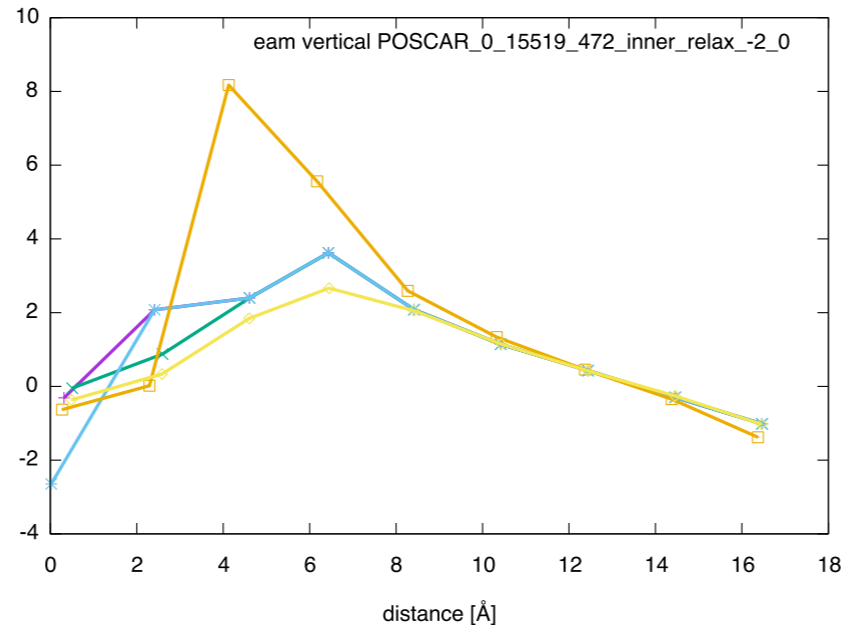
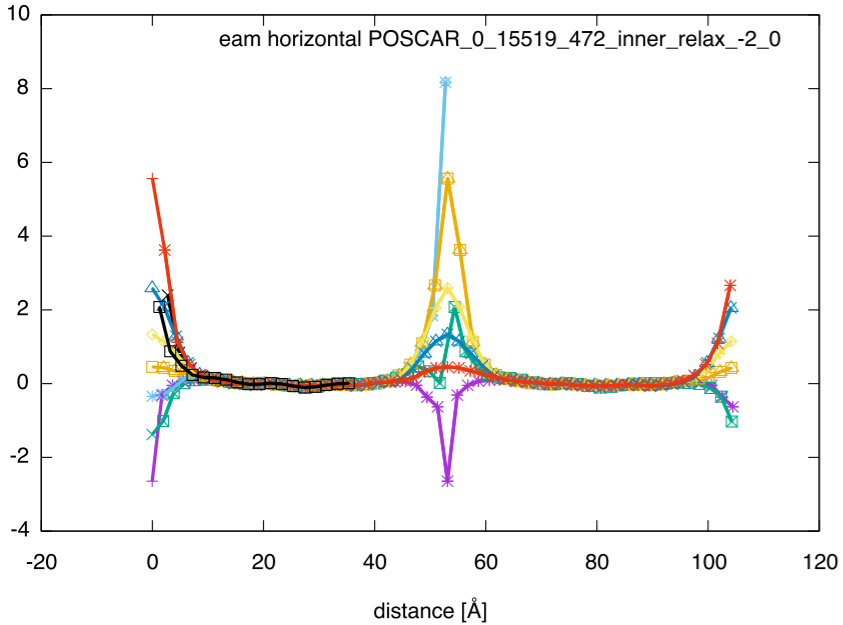
$$E_{\text{total}} = n A_0 \exp(-pr_0) - \sqrt{n} B_0^2 \exp(-2qr_0)$$

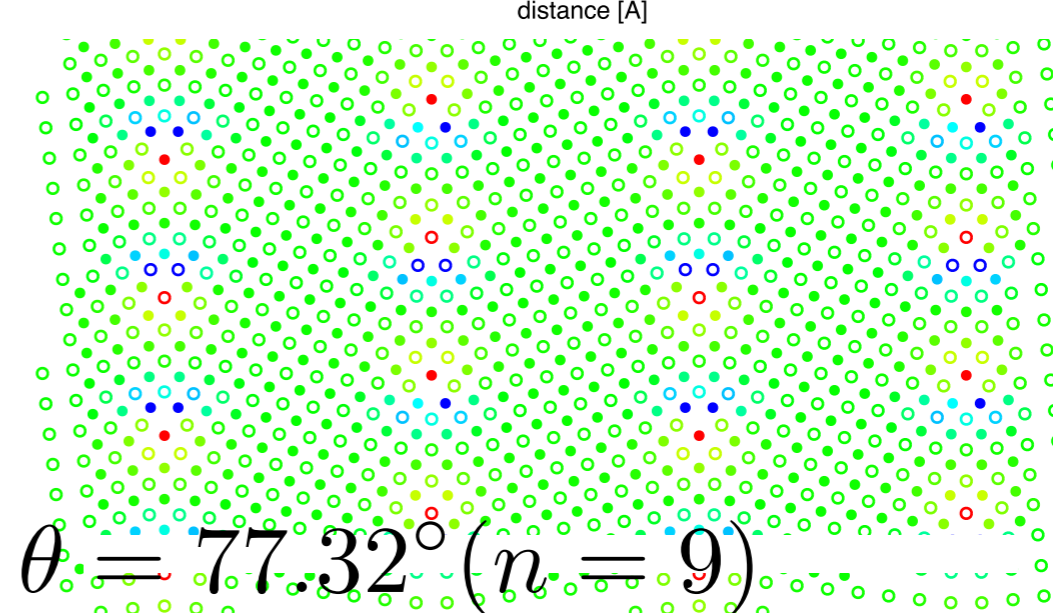
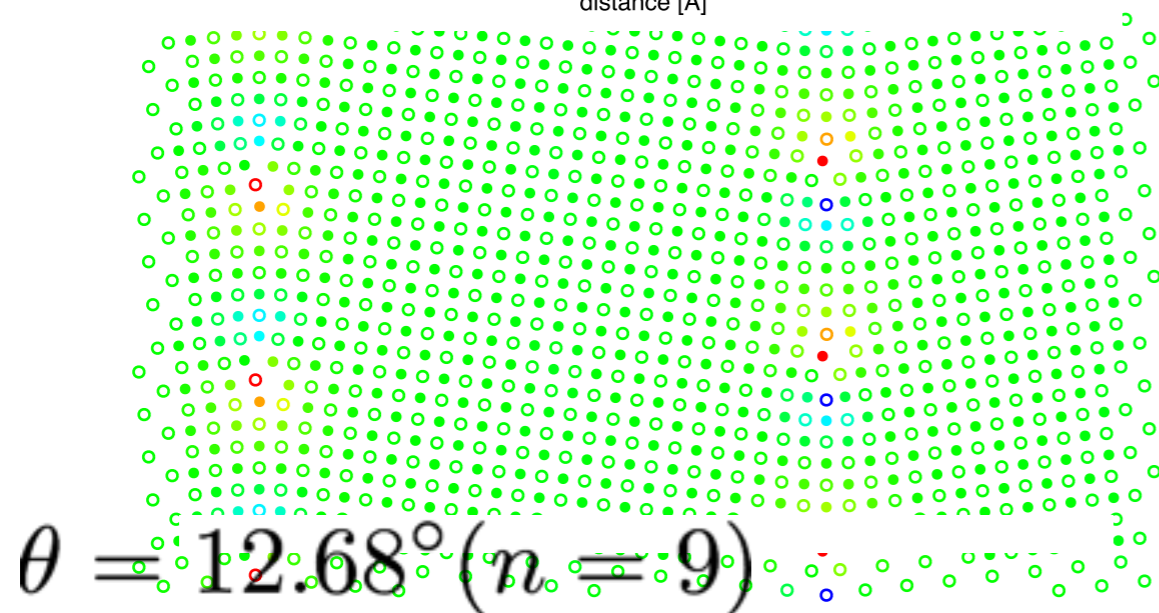
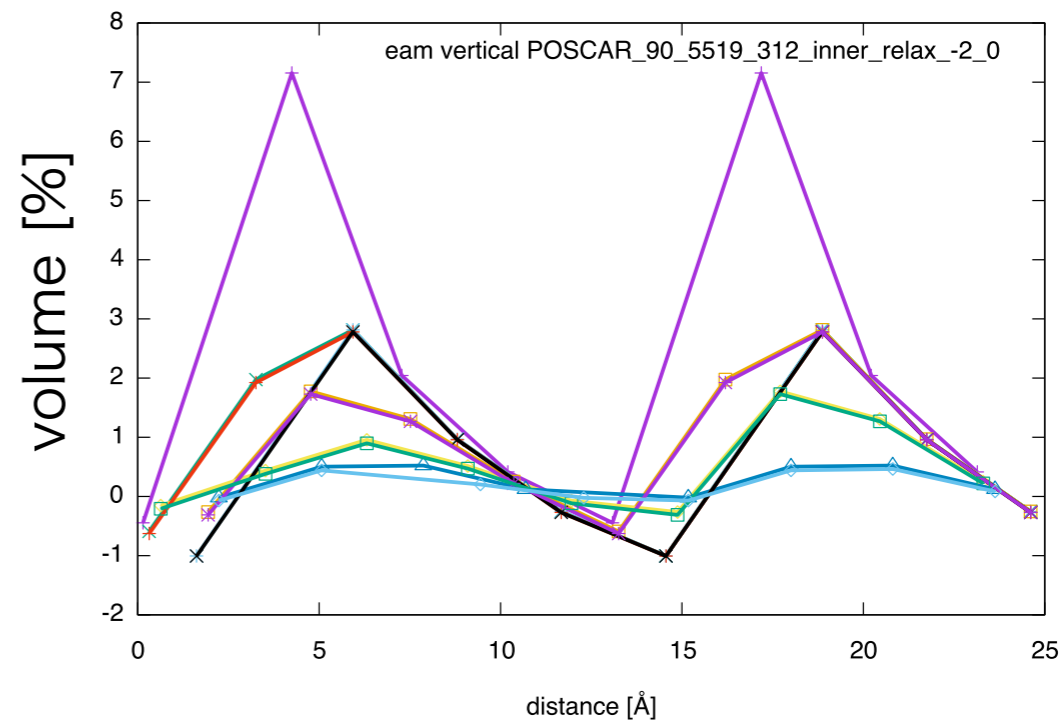
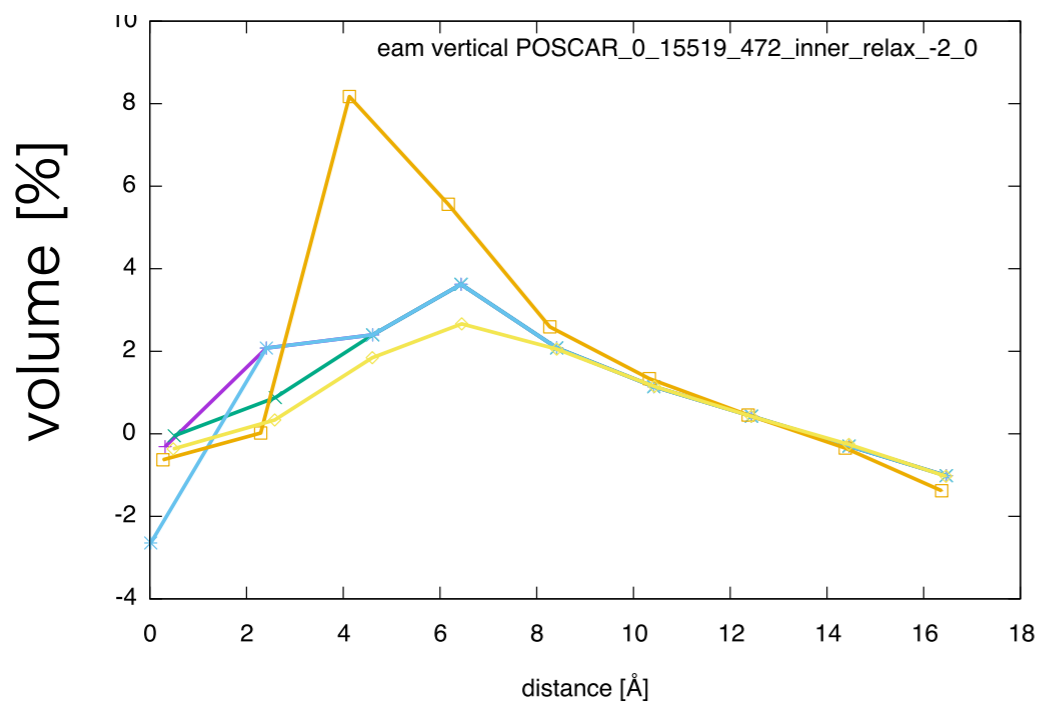
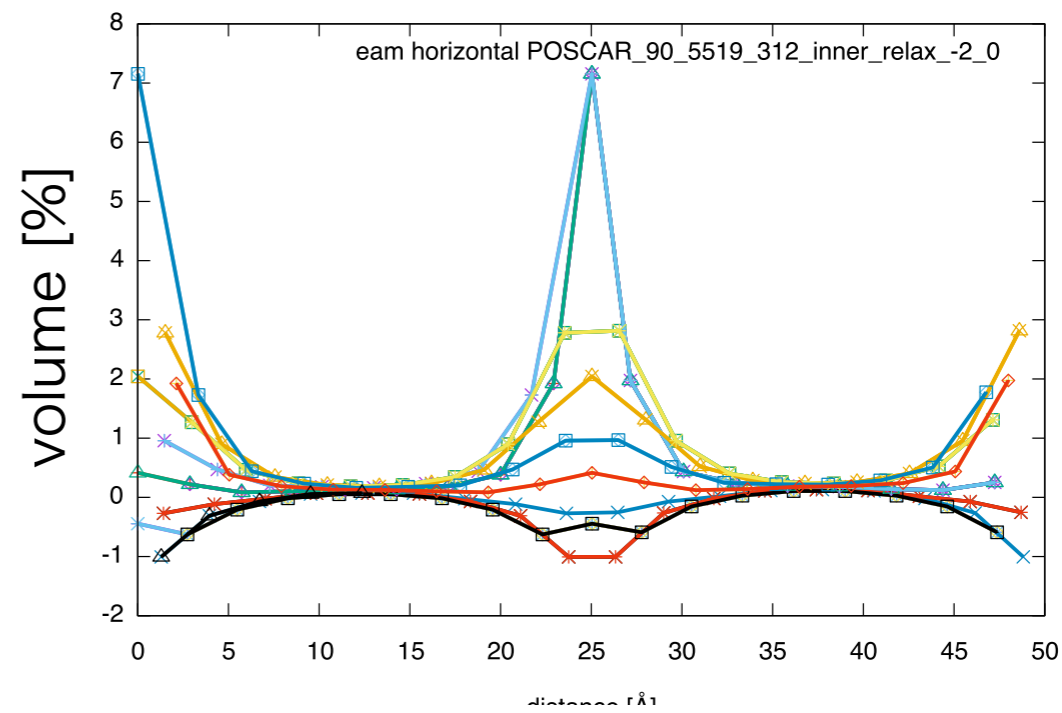
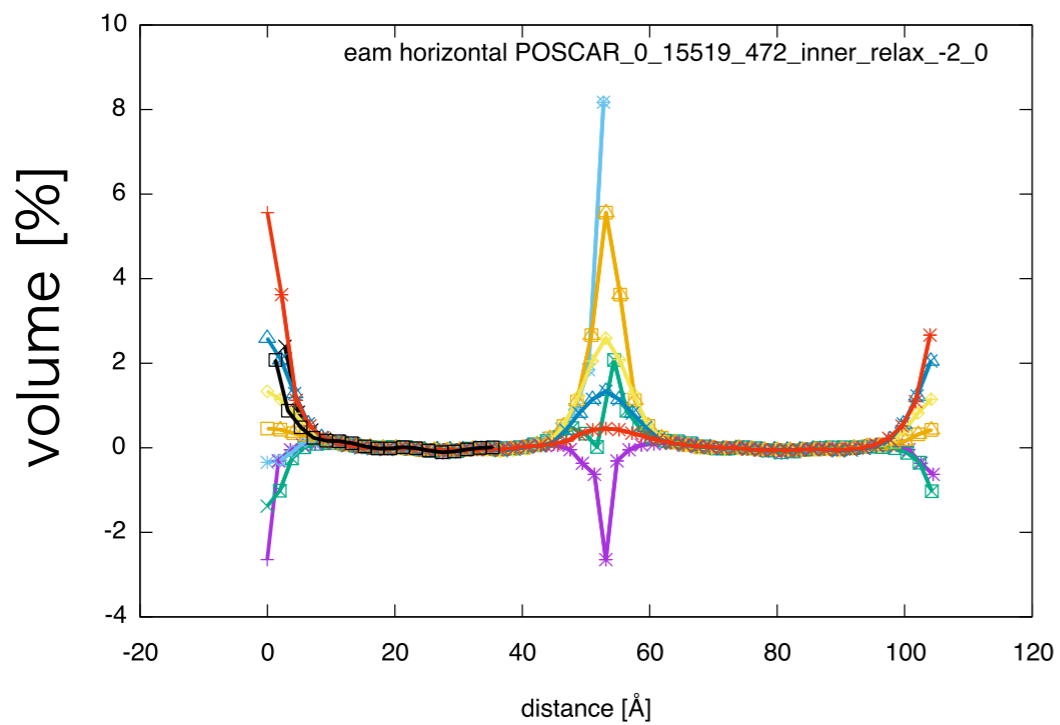
# Minimum energy and distance for Al EAM



> ruby plot\_minimum.rb







# Temporary conclusions

- Small angle Al and Cu(100) tilt boundary shows difference on the slopes at 0 and 90 degrees.
- Inconsistent with experiments results.
- Need smaller angle, larger super cell, model.